

NEW INVESTIGATIONS OF VON NEUMANN  
TYPE FLUIDS

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## Abstract

This paper presents some recent computer studies of a von Neumann type fluid. The particular model and the discrete dynamical equations utilized are described in detail and various results from fluid mechanics and statistical mechanics are discussed. Computer examples are presented and the model is shown to behave like a liquid as regards density, inter-particle separation, and surface wave generation.

## I. Introduction

During the late nineteen thirties, John von Neumann "became interested in questions of theoretical hydrodynamics, particularly in the great difficulties encountered in obtaining solutions to partial differential equations by known analytical methods." [1] From his studies, von Neumann published a paper [2] which described a new numerical method, discrete rather than continuous, for treating a class of hydrodynamic problems. In this approach, a quasi-molecular fluid model is developed in which the number of particles involved is reduced from that of a real fluid ( $\sim 10^{23}$ ) to a much more manageable number ( $\sim 10$ -100). In order that the smaller number of particles have the appropriate hydrodynamic behavior, the interparticle forces are adjusted and the physical parameters of each particle are modified. In a self-contained fashion, then, the present paper builds upon the results of an earlier paper [3] and extends the study of what has come to be called a von Neumann type fluid.

## II. Basic Approach

The following physical situation provides a starting point for the computer model. A liquid is poured into a right-circular cylindrical container. Initially, on the macroscopic level, it's behavior will be quite violent and erratic. Splashing and various wave phenomena will occur. After the passage of time, the fluid will settle down and stabilize. A definite top surface will develop and motion, at least at the macroscopic level, will subside. Within the fluid itself, on the microscopic level,

density and pressure gradients will arise and some particle motion will continue.

In order to model this situation numerically, we will proceed as follows: adopting the modern physical viewpoint, [4], [5], the liquid is assumed to be composed of interacting particles. Our original liquid contained 300 particles. This number was later reduced to 278, for reasons to be explained. The mass of each particle was taken to be 1.0 (CGS units are used throughout). The container itself was 10.0 units in diameter. A cylinder was chosen so that, by taking advantage of symmetry, only two-dimensional motion need be considered, i.e., the model represents a section through the vertical axis of the container. Particles were entered into the container with random positions and velocities and sufficient time was allowed for the liquid to settle. The average kinetic energy per particle was observed periodically and the liquid was deemed to have stabilized when further variations of this quantity was small. Liquid viscosity was taken into account at the container's boundaries by damping the velocity of any particle striking a wall to 10% of its original value. This damping factor is, of course, strictly a function of the material nature of the walls of the cylinder. Two different types of forces are allowed to act on and within the fluid. The forces between the particles are taken to be classical molecular in nature [5] and derivable from the Lennard-Jones potential. When any two particles are far away from each other, they experience an attractive force. As they approach each other, the attractive force is superceded by a much stronger repulsive force. Ultimately, these forces reach a relative state of equilibrium within the fluid. The entire fluid mass also experiences the force of gravity.

### III. Dynamical Equations

In implementing the general approach described in Section II, let the computer generated liquid be composed of  $N$  particles, denoted  $P_1, P_2, \dots, P_N$ , each of the same mass  $m$ . For positive time step  $\Delta t$ , let  $t_k = k\Delta t$ ,  $k = 0, 1, 2, 3, \dots$ . The state of the liquid will be described completely by giving the position and velocity of each particle for every time  $t_k$ . At each time  $t_k$ , let particle  $P_i$  be located at  $\vec{r}_{i,k} = (x_{i,k}, y_{i,k})$  and have velocity  $\vec{v}_{i,k} = (v_{i,k,x}, v_{i,k,y})$ . Furthermore, at  $t_k$  let  $P_i$  experience an acceleration  $\vec{a}_{i,k} = (a_{i,k,x}, a_{i,k,y})$ .

Let the position, velocity, and acceleration be related by the "leap-frog" formulas [6, p. 107]:

$$(3.1) \quad \vec{v}_{i, \frac{1}{2}} = \vec{v}_{i,0} + \frac{\Delta t}{2} \vec{a}_{i,0}$$

$$(3.2) \quad \vec{v}_{i, k+\frac{1}{2}} = \vec{v}_{i, k-\frac{1}{2}} + (\Delta t) \vec{a}_{i,k}, \quad k = 1, 2, 3, \dots$$

$$(3.3) \quad \vec{r}_{i, k+1} = \vec{r}_{i,k} + (\Delta t) \vec{v}_{i, k+\frac{1}{2}}, \quad k = 0, 1, 2, \dots$$

One should note that since these formulas generate positions at time  $t_k$  and velocities at times  $t_{k+\frac{1}{2}}$ , position and velocity are never known simultaneously. This precludes computing the total energy at each step. At any time step, one can compute either kinetic energy or potential energy, but not both.

At  $t_k$ , let the force acting on  $P_i$  be  $\vec{F}_{i,k} = (F_{i,k,x}, F_{i,k,y})$ .

We assume that force and acceleration are related by the discrete Newton's law

$$(3.4) \quad \vec{F}_{i,k} = m \vec{a}_{i,k}.$$

As soon as one specifies the form of  $\vec{F}_{i,k}$ , the motion of each particle, and hence the state of the liquid, will be determined recursively and explicitly by (3.1)-(3.4) from given initial data. The force  $\vec{F}_{i,k}$  is defined as follows. Let  $r_{ij,k} = |r_{i,k} - r_{j,k}|$  be the distance between  $P_i$  and  $P_j$  at time  $t_k$  and let  $G$  (coefficient of attraction),  $a$  (exponent of attraction),  $H$  (coefficient of repulsion), and  $b$  (exponent of repulsion) be given constants subject to the constraints  $G \geq 0$ ,  $H \geq 0$ ,  $b \geq a \geq 2$  [5]. Then the force  $\vec{F}_{i,k} = (\bar{F}_{i,k,x}, \bar{F}_{i,k,y})$  exerted by  $P_j$  on  $P_i$  is assumed to be

$$(3.5) \quad \bar{F}_{i,k,x} = m^2 \left\{ -\frac{G}{(r_{ij,k})^a} + \frac{H}{(r_{ij,k})^b} \right\} \frac{x_{i,k} - x_{j,k}}{r_{ij,k}}$$

$$(3.6) \quad \bar{F}_{i,k,y} = m^2 \left\{ -\frac{G}{(r_{ij,k})^a} + \frac{H}{(r_{ij,k})^b} \right\} \frac{y_{i,k} - y_{j,k}}{r_{ij,k}}.$$

The total force  $(F_{i,k,x}^*, F_{i,k,y}^*)$  on  $P_i$  due to all the other particles is given by summing over the expressions (3.5)-(3.6), excluding the  $i$ th term:

$$(3.7) \quad F_{i,k,x}^* = \sum_{\substack{j=1 \\ j \neq i}}^N \bar{F}_{i,k,x}, \quad F_{i,k,y}^* = \sum_{\substack{j=1 \\ j \neq i}}^N \bar{F}_{i,k,y}.$$

The force of gravity is given by  $(0, -980m)$ . Adding this to (3.7) gives us the final expression for  $\vec{F}_{i,k}$ :

$$(3.8) \quad F_{i,k,x} = F_{i,k,x}^*; \quad F_{i,k,y} = F_{i,k,y}^* - 980m$$

In liquids, all particles are always within the strong force fields of their neighbors [7, p. 46]. Furthermore, it is known "that the "inter-molecular forces are shortranged, [with] interaction between molecules hardly extending beyond nearest neighbors." [8, p. 225] To emphasize the localness of particle interactions, only those particles within a fixed distance  $r_0$  of  $P_i$  are allowed to contribute to the attractive and repulsive forces experienced by  $P_i$ . Besides being physically reasonable, allowing such local interactions makes for much faster computation times. With  $N$  particles there are  $N(N-1)/2$  total interactions. Clearly, if this number can be appreciably reduced, the expressions (3.5)-(3.6) will be evaluated less often, and the computer code will be more efficient numerically.

Particle damping and rebounding from the container walls is implemented as follows. Let one end of the base of our rectangular section be at the origin  $(0,0)$  and let the other end be at  $(A,0)$ . Then

- (a) if  $x_{i,k} < 0$ , reset  $P_i$  at  $(-x_{i,k}, y_{i,k})$
- (b) if  $x_{i,k} > A$ , reset  $P_i$  at  $(2A - x_{i,k}, y_{i,k})$
- (c) if  $y_{i,k} < 0$ , reset  $P_i$  at  $(x_{i,k}, -y_{i,k})$ .

Suppose that  $P_i$  has velocity  $\vec{v}_{i,k}^*$  at  $t_k$ . After resetting the position, one resets the velocity to  $\vec{v}_{i,k}$ , where

- (a) if  $x_{i,k} < 0$  or  $x_{i,k} > A$ ,  $\vec{v}_{i,k} \rightarrow (1-d)(-v_{i,k,x}^*, v_{i,k,y}^*)$   
(b) if  $y_{i,k} < 0$ ,  $\vec{v}_{i,k} \rightarrow (1-d)(v_{i,k,x}^*, -v_{i,k,y}^*)$ ,

where  $d$  is a fixed damping constant. After extensive computer experimentation, the following parameter selections were settled upon:  $N = 300$  (later 278),  $A = 10.0$ ,  $G = 25.0$ ,  $a = 2$ ,  $H = 50$ ,  $b = 4$ ,  $m = 1.0$ ,  $d = 0.9$ ,  $r_0 = 0.25$ , and  $\Delta t = 10^{-4}$ . The time step is chosen so as to satisfy the condition  $\Delta t \ll \frac{r}{\|\vec{v}_{i,k}\|}$  for every  $i$  and every  $k$  [9, p. 123]. In general,  $r$  is taken to be a typical interaction distance. Here,  $r = r_0$  was used. Time steps larger than  $10^{-4}$  were tried with the result being, typically, the onset of instability. (The exact FORTRAN code which implements the model with the parameter choices given above is given in Appendix I of [10].)

Before any investigation of the liquid computer model can begin, a stable, settled configuration must be attained. Ideally, one could determine a stable initial state for every possible choice of parameters. This problem, however, is entirely intractable mathematically. Consequently, it is necessary to allow the liquid to find its own stable particle distribution. This is done by placing the particles at random positions in the container and giving them random velocities and then by observing the state of the fluid at successive time steps. This was done and, as time passed, the fluid was observed to stabilize from the bottom up with a new layer of 40 particles appearing approximately every .17 to .22 units. During this phase of the computations, it was felt that if this trend were to continue, 20 of the 300 particles would not fit into

any level. Hence, the number of particles was reduced from  $N = 300$  to  $N = 280$ . This, we believed, would result in a liquid of 7 levels with 40 particles in each level. After allowing about 21 seconds of physical (fluid) time to pass, the topmost row refused to conform and level out. A good deal of activity continued after the remainder of the liquid had settled. It was concluded that this surface activity was appropriate and reflected molecular activity, like Brownian motion and evaporation, which occur in a real liquid at the surface/external medium interface. [4] Ultimately, two particularly incorrigible particles were removed. The result was a stable liquid of 278 particles. This particle arrangement can be seen in Fig. 1. The average kinetic energy per particle is 20.467. (The exact positions and velocities are given in Appendix II of [10].)

#### IV. Qualitative Nature of the Modeled Fluid

An interesting, but very difficult, question to consider is whether we have modeled a liquid or a gas. Let us now examine some of the various approaches to answering this question. One of them, for example, is statistical. It is known that "in assemblies where particles interact with short-range forces, of the order of 1,000 particles are sufficient to exhibit statistical behavior." [9, p. 122] With this number of particles, one can average over individual particle motions and speak meaningfully of the fluid's temperature, pressure, viscosity, thermal conductivity, and other thermodynamic properties. [11] One would then be able to compare values computed statistically against those computed experimentally for real liquids and gases. In this way, one would not only be able to

distinguish between a liquid and a gas but would hopefully be able to specify the particular liquid or gas actually modeled.

An example of a specific difference between liquids and gases, arising out of statistical behavior, which would be testable readily, given a suitable number of particles, is the following. For homogeneous and incompressible fluids (liquids), pressure is proportional to depth while for gases, the natural logarithm of pressure is proportional to depth. [12, p. 31-32] One could graph these quantities to see which hypothesis, liquid or gas, best explains the data. A drawback to this approach is, of course, the large number of particles required. Limited

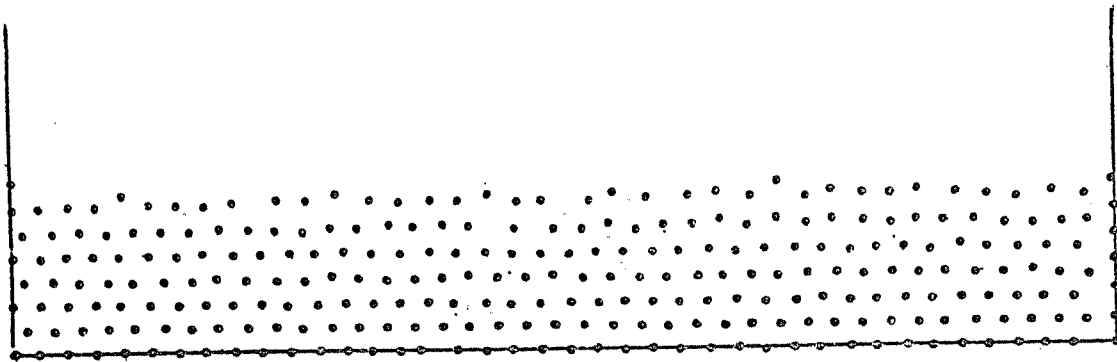


FIGURE 1 - Settled Fluid

funds and a lack of sufficiently powerful computing machinery have so far prevented our modeling of fluids of this size. However, other approaches to be described next, and which are based upon less formal properties, are available and do imply that our fluid is a liquid.

It is known [7, p. 45-46] that the average particle separation in a typical gas is of the order of  $10d$  where  $d$  is the equilibrium distance at which attraction and repulsion balance. In a liquid, the average particle separation is of the order of  $d$ . For the particular choice of parameters used in this paper,  $d$  is 1.414. For the fluid presented in Fig. 1, the mean separation is 0.255. This is evidence in favor of the fluid generated being a liquid. Furthermore, "liquids can be regarded for most purposes as being incompressible." [7, p. 76] This means that further evidence for a liquid-like nature rather than a gaseous nature is the property of uniform particle density. Consideration of Table I shows a remarkably uniform distribution of particles. (The uppermost 39 particles at the surface have been excluded.)

| TABLE I         |                     |
|-----------------|---------------------|
| Range in Height | Number of Particles |
| 0.0 - 0.2       | 40                  |
| 0.2 - 0.4       | 40                  |
| 0.4 - 0.6       | 40                  |
| 0.6 - 0.8       | 40                  |
| 0.8 - 1.0       | 39                  |
| 1.0 - 1.2       | 40                  |

Another approach in the consideration of the type of fluid actually generated comes from the observation of the fluid's macroscopic properties.

Earlier studies of a von Neumann type fluid have demonstrated the properties of bouyancy, expansion due to heating, convection, free surface flow, and cavity flow. [3, 13] We next add to this list splashing and surface wave generation which result when a particle of greater relative mass is dropped into the fluid, from which will follow, again, the liquid nature of our fluid. Incidentally, the computer examples which follow are also of interest in themselves, since they describe the evolution of fundamental fluid phenomena.

#### V. Splashing and Surface Wave Generation

After a stable configuration had been obtained, a single additional particle was added to the other 278. This new particle,  $P_{279}$ , was placed above the surface at (5,1.7), released, and allowed to drop into the fluid. Three cases were considered: 1) particle has mass = 10.0 and initial velocity zero, 2) particle has mass = 10.0 and initial velocity of 30.0 downward, and 3) particle has mass = 250.0 and initial velocity zero.

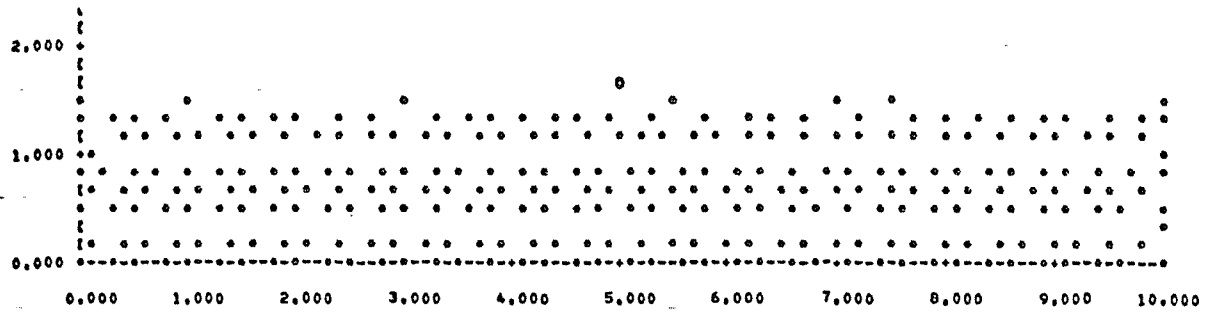
Graphs of the resulting fluid motions are shown in Figures 2-4, and these will be discussed separately. Note first, however, that due to limitations of printer spacing, gaps appear in the automatic plots given in Figures 2-4 which do not actually occur in the fluid or in the computer output. This shortcoming is apparent immediately by comparing Figure 1 and Figure 2(a). The only difference that exists between these two graphs is the existence of particle  $P_{279}$  in Figure 2(a). Otherwise, the two graphs are of the identical fluid. Figure 1, however, was drawn by hand and is the more accurate of the two.

Figures 2(a)-(e) show the effect of dropping  $P_{279}$ , of mass 10.0, from a position of rest, into the fluid. The resulting motion is shown, respectively, at times  $t_0$ ,  $t_{229}$ ,  $t_{503}$ ,  $t_{823}$ , and  $t_{1143}$ . This gentle drop into the fluid results in the splash effect which is seen clearly in Figure 2(c). The splash continues to increase in size, as is shown in Figure 2(d), while the rate of descent of  $P_{279}$  slows. Simultaneously,  $P_{279}$  is covered over by fluid particles. Figure 2(e) shows the fall of the two waves generated by the splash.

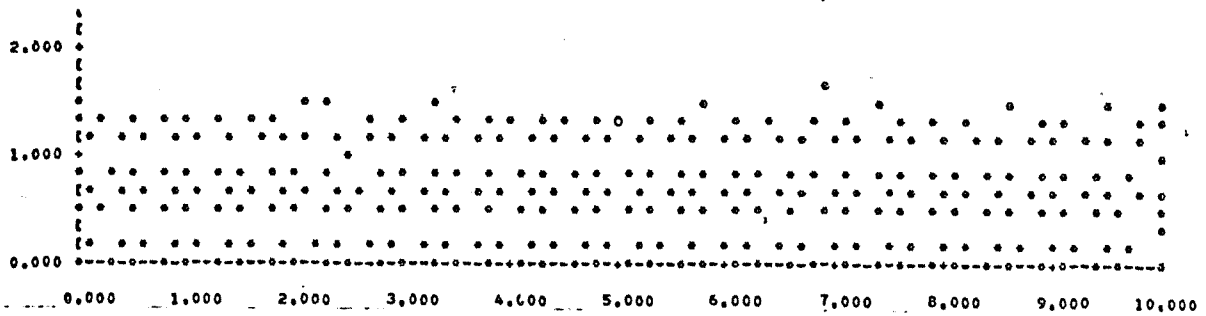
To accentuate the effects shown in Figure 2, we next reset the velocity of  $P_{279}$  to  $(0, -30)$ . The results of this change are shown in Figures 3(a)-(d) at the respective times  $t_{137}$ ,  $t_{229}$ ,  $t_{824}$ , and  $t_{1464}$ . Figures 3(a) and (b) show a more rapid entry and descent than those shown in Figure 2. Figures 3(c) and (d) show the generation of outward moving waves at the later times  $t_{824}$  and  $t_{1464}$ .

In order, again, to accentuate the effects shown in Figure 2,  $P_{279}$  was once more dropped from a position of rest, but this time its mass was set at the extreme value  $m = 250$ . Figures 4(a) and (b), at the respective times  $t_{229}$  and  $t_{366}$ , show a more rapid rate of descent within the fluid and a much larger splash than that shown in Figure 2. However, it is likely that extensive calculation with such a large mass might require decreasing the time step  $\Delta t$ , since interparticle forces can now be exceptionally large.

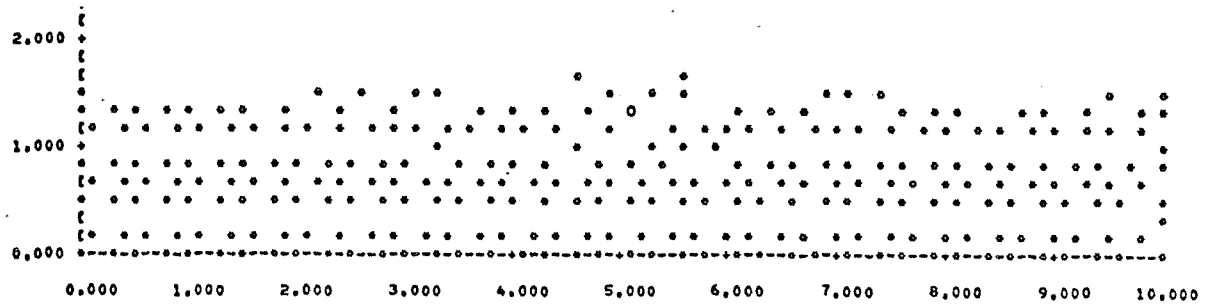
In all three cases described above, note that the physical reactions are consistent with the contention that the fluid is a liquid.



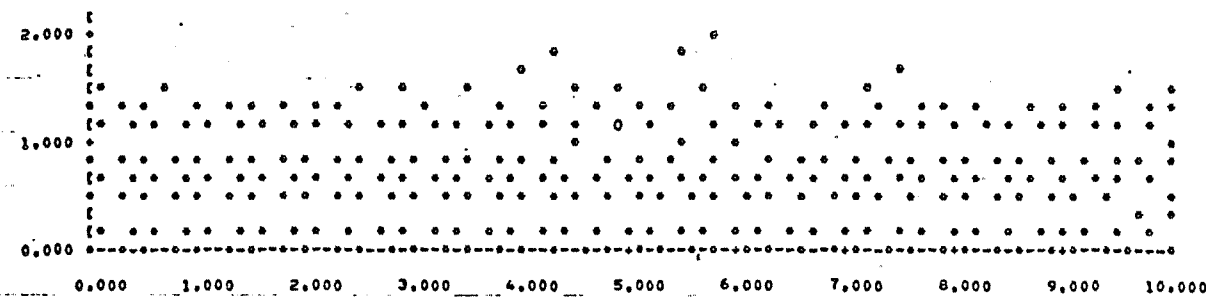
(a)



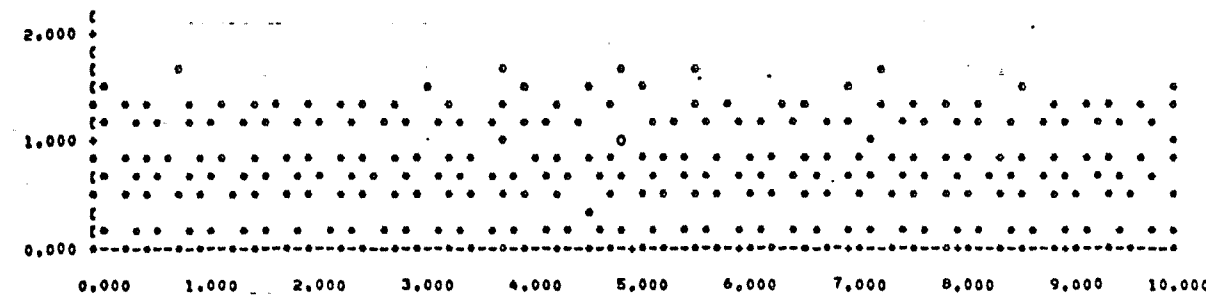
(b)



(c)

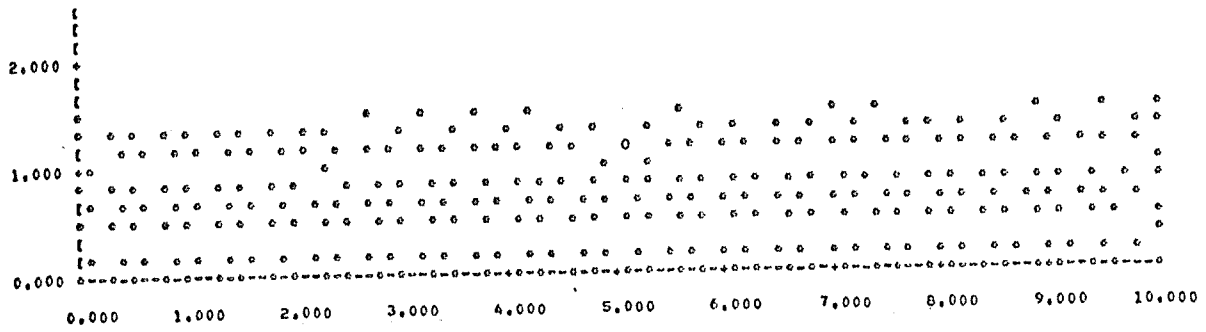


(d)

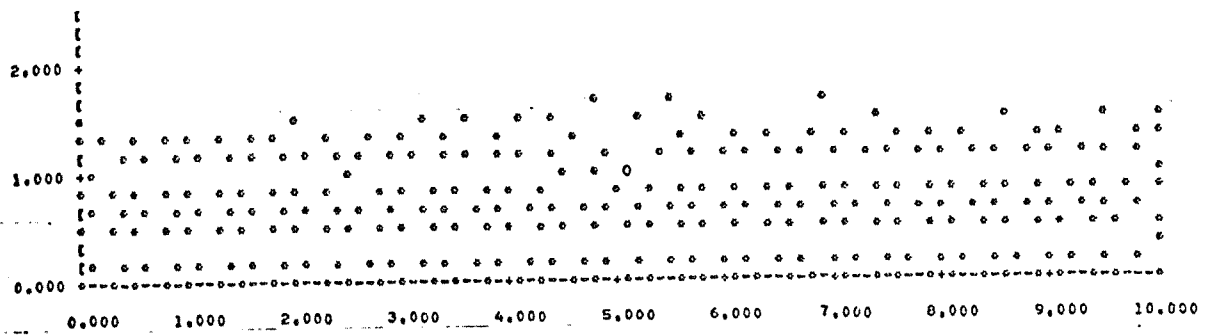


(e)

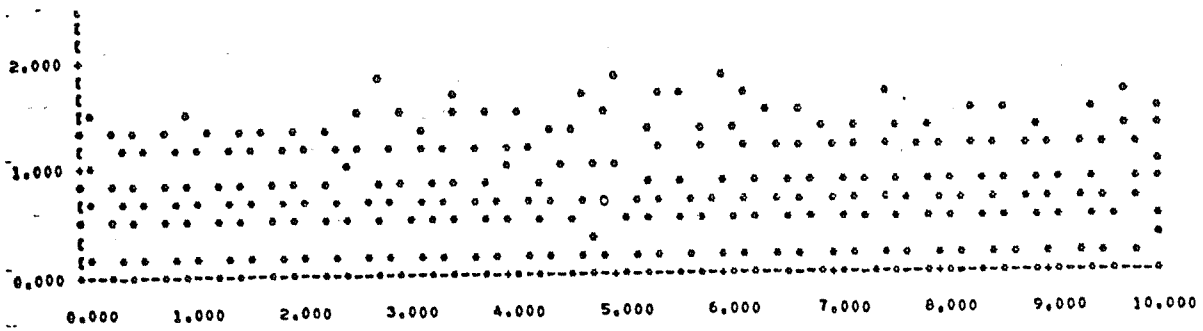
FIGURE 2



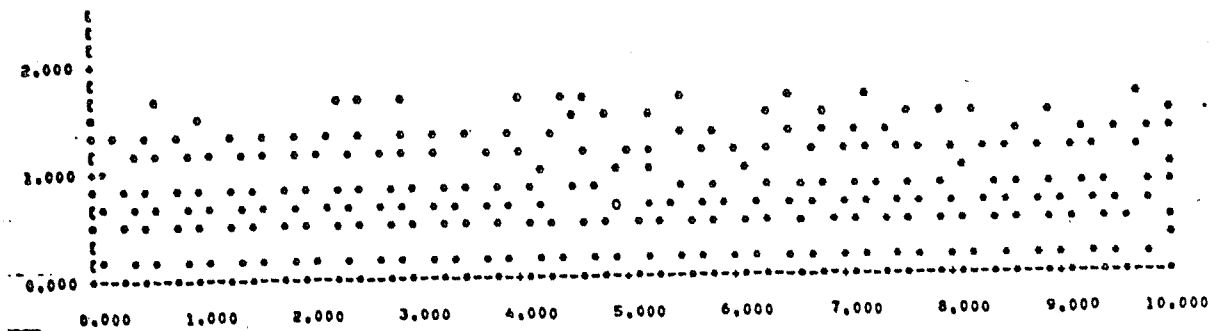
(a)



(b)



(c)



(d)

FIGURE 3

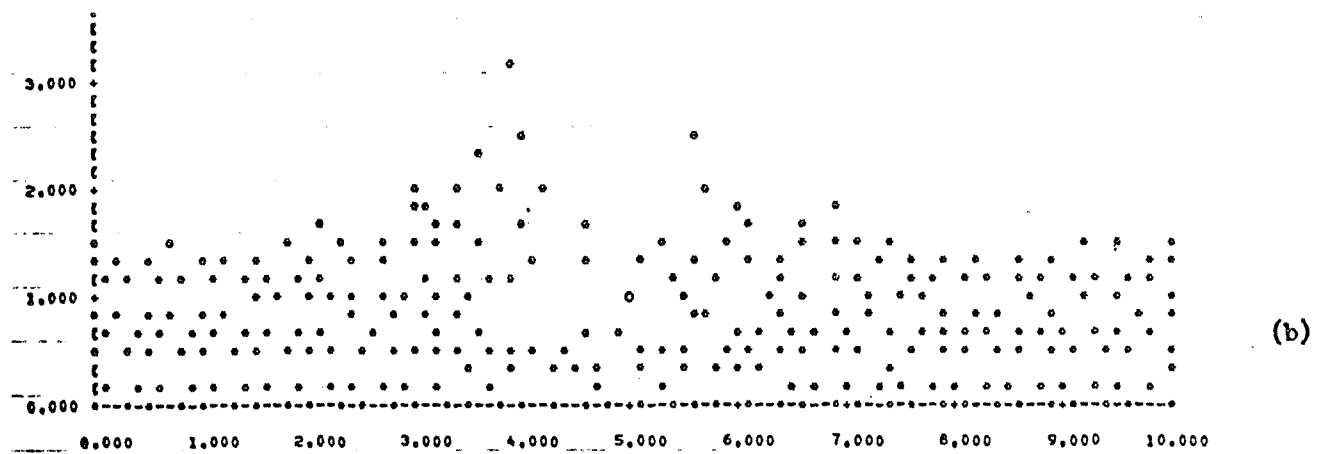
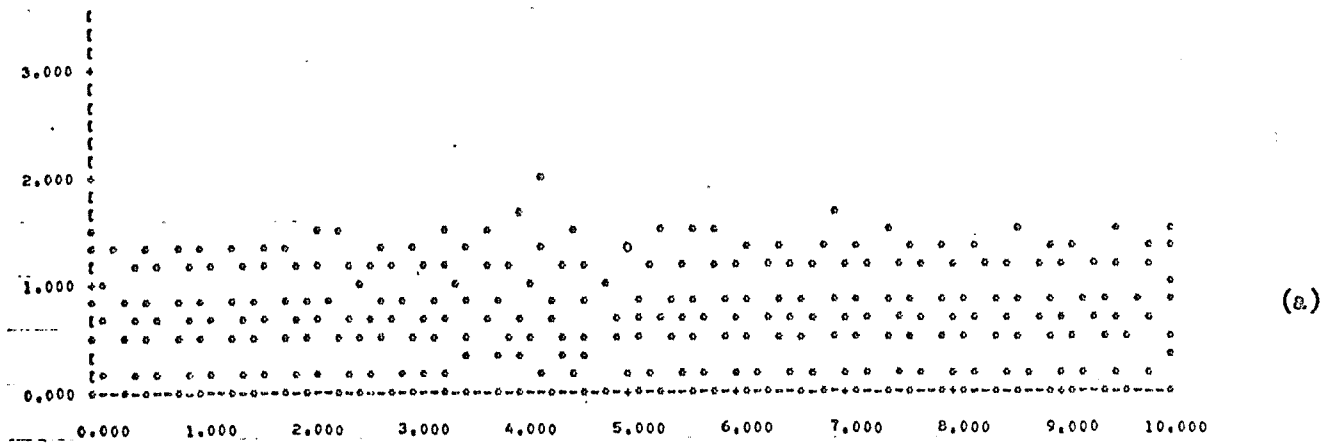


FIGURE 4

## V. Remarks

As was stated earlier, the liquid produced in this paper was the result of a great deal of experimentation in the selection of parameter values. Table II shows some of the parameter combinations and the nature of the density of the resulting fluid.  $N$  is the number of particles in the fluid,  $w$  is the width of the container,  $d$  is the depth of the fluid,  $r_0$  is the radius of interaction, mean sep. is the mean separation of particles, and  $KE/p.$  is the mean kinetic energy per particle. All fluids have particle masses of 2.5.

While none of these earlier combinations generated a fluid with uniform density, a few of them, 4 and 10 for example, could be called heavy gases. (For exact positions and velocities, see Appendices III and IV of [10].) As such, they would prove useful in simulating the earth's atmosphere.

If the force expression contains only repulsion, it is reasonable to expect the resulting fluid to be gaseous in nature. This conclusion follows from the fact that "at the molecular level a perfect gas is characterized by the absense of intermolecular attraction." [7, p. 345] Fluids 2 through 5, which resulted solely from repulsive forces, do indeed have the compressibility which is characteristic of gases.

Not all of the fluids given in Table II were run to stability. In order to save time, some computations were stopped when it became clear that a particular set of parameters was not moving towards a liquid.

Table II

|    | N   | H   | b | G  | a | w  | d   | $r_0$ | mean<br>sep. | KE/p.  | nature of density                         |
|----|-----|-----|---|----|---|----|-----|-------|--------------|--------|-------------------------------------------|
| 1  | 300 | 1   | 3 | 0  | - | 6  | 1.2 | -     | .13          | .46    | irregular                                 |
| 2  | 267 | 25  | 3 | 0  | - | 6  | 5   | -     | .36          | 4.62   | increasing downward                       |
| 3  | 267 | 50  | 3 | 0  | - | 6  | 8.5 | -     | .45          | 64.03  | increasing downward<br>thin at top        |
| 4  | 267 | 100 | 3 | 0  | - | 6  | 10  | -     | .50          | .69    | gradual increase<br>downward              |
| 5  | 300 | 1   | 5 | 0  | - | 6  | 3.5 | -     | .25          | .28    | increasing downward                       |
| 6  | 582 | 1   | 5 | 0  | - | 10 | 2.6 | -     | .25          | .33    | irregular                                 |
| 7  | 300 | 1   | 5 | 1  | 2 | 6  | 2.5 | -     | .24          | .03    | increasing downward<br>irregular near top |
| 8  | 267 | 100 | 3 | .5 | 6 | 6  | 10  | -     | .50          | .58    | gradual increase<br>downward              |
| 9  | 267 | 100 | 3 | 10 | 2 | 6  | 9   | -     | .48          | .67    | increasing downward<br>some irregularity  |
| 10 | 300 | 100 | 3 | 75 | 2 | 6  | 5.5 | 2     | .34          | 47.20  | gradual increase<br>downward              |
| 11 | 300 | 100 | 4 | 75 | 2 | 6  | 7   | 1.5   | .40          | 34.54  | irregular                                 |
| 12 | 300 | 50  | 5 | 25 | 2 | 6  | 5   | 1.5   | .34          | 108.00 | irregular                                 |
| 13 | 247 | 50  | 5 | 25 | 3 | 10 | 4   | 2     | .43          | 3.45   | irregular                                 |
| 14 | 300 | 50  | 5 | 25 | 3 | 6  | 8   | 2     | .46          | 88.17  | irregular                                 |
| 15 | 300 | 50  | 5 | 25 | 3 | 10 | 6   | 2     | .46          | 86.87  | irregular                                 |
| 16 | 300 | 50  | 6 | 25 | 2 | 6  | 5.7 | 1.5   | .37          | 264.49 | uniform in mid-<br>section                |

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## APPENDIX I

### FORTRAN PROGRAM

```

1 C *****
2 C *
3 C   THIS PROGRAM IS DESIGNED TO MODEL THE BEHAVIOR OF A FLUID IN A
4 C   CONTAINER. A LEAP-FROG FORMULATION IS BEING USED.
5 C *
6 C *****
7
8   INTEGER CF
9   REAL MASS
10  DIMENSION X(280),Y(280),VX(280),VY(280),FX(280),FY(280)
11  COMMON X,Y,VX,VY,NPARTS,WIDTH,HEIGHT,TIME,K,KK
12  COMMON /MNRTST/ CF
13  IF(LINKME(0,7).LT.0) STOP NOLNK7
14  IF(LINKME(1,6).LT.0) STOP NOLNK6
15
16 C ->  PARAMETER DEFINITION
17
18     MASS=1.0
19     DT=0.0001
20     DTM=DT/MASS
21     NTIME=1000000
22
23 C ->  RESTART THE PROGRAM USING THE APPROPRIATE 'STARTING FORMULA'. THIS
24 C ->  PORTION OF THE PROGRAM REPRESENTS STARTING THE COMPUTATION AT K=0.
25
26     CALL RSTART
27     CALL FORCE(FX,FY)
28     DO 1 I=1,NPARTS
29         VX(I)=VX(I)+0.5*DTM*FX(I)
30         VY(I)=VY(I)+0.5*DTM*FY(I)
31         X(I)=X(I)+DT*VX(I)
32         Y(I)=Y(I)+DT*VY(I)
33
34 C ->  ADJUST POSITIONS AND VELOCITIES TO TAKE INTO ACCOUNT ANY
35 C ->  COLLISIONS WHICH HAVE OCCURRED WITH THE WALLS OF THE CONTAINER.
36
37         IF((X(I).GT.WIDTH).OR.(X(I).LT.0.0).OR.(Y(I).LT.0.0))
38     +     CALL CNTAIN(I)
39
40     1 CONTINUE
41     K=K+1
42
43 C ->  MOVE AHEAD FROM STEP K TO STEP K+1 AND COMPUTE NEW POSITIONS AND
44 C ->  VELOCITIES.
45
46     DO 3 KK=K,NTIME
47         TIME=TIME+DT
48         CALL FORCE(FX,FY)
49
50         DO 2 I=1,NPARTS
51             VX(I)=VX(I)+DTM*FX(I)
52             VY(I)=VY(I)+DTM*FY(I)
53             X(I)=X(I)+DT*VX(I)
54             Y(I)=Y(I)+DT*VY(I)
55

```

```

56      IF((X(I).GT.WIDTH).OR.(X(I).LT.0.0).OR.(Y(I).LT.0.0))
57      *      CALL CNTAIN(I)
58
59
60      2 CONTINUE
61      IF(MOD(KK,50).EQ.0) CALL STORE
62      3 CONTINUE
63      STOP OK
64      END
65
66
67      S U B R O U T I N E STORE
68
69 C *****
70 C *
71 C      STORE STORES THE MOST RECENT DATA AND PARAMETERS ON LOGICAL UNIT
72 C      NUMBER '35 AND '36.
73 C *
74 C *****
75
76      INTEGER CF,PAR(20)
77      DIMENSION X(280),Y(280),VX(280),VY(280)
78      DIMENSION LUNFLE(2),NF(2)
79      COMMON X,Y,VX,VY,NPARTS,WIDTH,HEIGHT,TIME,K,KK
80      COMMON/MNRTST/CF
81      DATA LUNFLE/'35','36/'
82      DATA NF/2,1/
83
84      L=KK
85      WRITE('34,1) NPARTS,L,WIDTH,HEIGHT,TIME,CF
86      1 FORMAT(2I7,3E15.7,I1)
87      DO 6 I=1,NPARTS
88      WRITE('34,2) X(I),Y(I),VX(I),VY(I)
89      2 FORMAT(4E15.7)
90      6 CONTINUE
91      END FILE '34
92      REWIND '34
93      CF=NF(CF)
94      LFLE=LUNFLE(CF)
95      REWIND LFLE
96      ICHECK=0
97      3 READ('34,4,END=5) (PAR(J),J=1,20)
98      ICHECK=ICHECK+1
99      WRITE(LFLE,4) (PAR(J),J=1,20)
100     GO TO 3
101     5 CONTINUE
102     IF(ICHECK.NE.NPARTS+1) STOP 1
103     END FILE LFLE
104     REWIND LFLE
105     REWIND '34
106     CLOSE 10
107     4 FORMAT(20A3)
108     RETURN
109     END
110

```

```

111
112      S U B R O U T I N E CNTAIN(I)
113
114 C *****
115 C *
116 C      DAMP = 1.0 IF DAMPING IS TOTAL
117 C      DAMP = 0.0 IF THERE IS NO DAMPING
118 C *
119 C *****
120
121      DIMENSION X(280),Y(280),VX(280),VY(280)
122      COMMON X,Y,VX,VY,NPARTS,WIDTH,HEIGHT,TIME,K,KK
123
124      DAMP=0.9
125      D1=0.1
126 C => D1 = 1.0 - DAMP
127
128      IF(X(I).LE.WIDTH) GO TO 1
129      X(I)=2.0*WIDTH-X(I)
130      VX(I)=-D1*VX(I)
131      VY(I)=D1*VY(I)
132      GO TO 2
133 1 IF(X(I).GE.0.0) GO TO 2
134      X(I)=-X(I)
135      VX(I)=-D1*VX(I)
136      VY(I)=D1*VY(I)
137 C 2 IF(Y(I).GE.0.0) RETURN
138 2 CONTINUE
139      IF(ABS(VX(I)).LT.1.0E-10) VX(I)=0.0
140      IF(Y(I).GE.0.0) RETURN
141      Y(I)=-Y(I)
142      VX(I)=D1*VX(I)
143      VY(I)=-D1*VY(I)
144      IF(ABS(VX(I)).LT.1.0E-10) VX(I)=0.0
145      RETURN
146      END
147
148
149      S U B R O U T I N E FORCE(FKX,FKY)
150
151 C *****
152 C *
153 C      FKX = FORCE ON PARTICLE IN X-DIRECTION
154 C      FKY = FORCE ON PARTICLE IN Y-DIRECTION
155 C      H = CONSTANT OF REPULSION
156 C      A = EXPONENT OF REPULSION
157 C      G = CONSTANT OF ATTRACTION
158 C      B = EXPONENT OF ATTRACTION
159 C *
160 C *****
161
162      DIMENSION X(280),Y(280),VX(280),VY(280),FKX(280),FKY(280)
163      COMMON X,Y,VX,VY,NPARTS,WIDTH,HEIGHT,TIME,K,KK
164      DO 1 M=1,NPARTS
165      FKX(M)=0.0

```

```

166      FKY(M)=0.0
167      1 CONTINUE
168      NPART1=NPARTS-1
169      DO 2 I=1,NPART1
170      IP1=I+1
171      DO 2 J=IP1,NPARTS
172      IF((ABS(X(I)-X(J)).GT.0.25).OR.(ABS(Y(I)-Y(J)).GT.0.25)) GO TO 2
173 C -> PARTICLES A DISTANCE FARTHER AWAY THAN 0.25 ARE NOT ALLOWED TO
174 C -> INTERACT.
175      RIJ2=(X(I)-X(J))*(X(I)-X(J))+(Y(I)-Y(J))*(Y(I)-Y(J))
176
177 C -> RIJ2 = SQUARED DISTANCE BETWEEN PARTICLE I AND PARTICLE J
178
179      IF(RIJ2.GT.(0.0625)) GO TO 2
180 C -> PARTICLES A DISTANCE FARTHER AWAY THAN 0.25 ARE NOT ALLOWED TO
181 C -> INTERACT.
182
183 C -> ONLY PARTICLES WITHIN A CERTAIN DISTANCE OF EACH OTHER ARE ALLOWED
184 C -> TO INTERACT.
185
186      RIJ4=RIJ2*RIJ2
187      Z=(( 50.0/RIJ4)-( 25.0/RIJ2))*1.0
188 C -> Z=((H/R**A)-(G/R**B))*MASS(I)*MASS(J)
189      RIJ=SQRT(RIJ2)
190      FX=Z*((X(I)-X(J))/RIJ)
191      FY=Z*((Y(I)-Y(J))/RIJ)
192      FKX(I)=FKX(I)+FX
193      FKX(J)=FKX(J)-FX
194      FKY(I)=FKY(I)+FY
195      FKY(J)=FKY(J)-FY
196      2 CONTINUE
197      DO 3 I=1,NPARTS
198      FKY(I)=FKY(I)-980.0
199 C -> ACCELERATION OF GRAVITY = 980.0CM/S**2
200 C -> CONSTANT TERM = MASS*980.0
201      3 CONTINUE
202      RETURN
203      END
204
205
206      S U B R O U T I N E RSTART
207
208 C *****
209 C *
210 C      RSTART READS THE MOST RECENT DATA AND PARAMETERS FROM LOGICAL UNIT
211 C      NUMBER '33.
212 C *
213 C *****
214
215      INTEGER CF,PAR(20)
216      DIMENSION X(280),Y(280),VX(280),VY(280)
217      COMMON X,Y,VX,VY,NPARTS,WIDTH,HEIGHT,TIME,K,KK
218      COMMON /MNRTST/ CF
219
220      REWIND '33

```

```
221      REWIND '35
222      REWIND '36
223      ICHECK=0
224      1 READ('35,80,END=2) (PAR(I),I=1,20)
225      ICHECK=ICHECK+1
226      WRITE('33,80) (PAR(I),I=1,20)
227      GO TO 1
228      2 IF(ICHECK.EQ.280) GO TO 5
229      ICHECK=0
230      REWIND '33
231      3 READ('36,80,END=4) (PAR(I),I=1,20)
232      ICHECK=ICHECK+1
233      WRITE('33,80) (PAR(I),I=1,20)
234      GO TO 3
235      4 IF(ICHECK.NE.280) STOP 4
236      5 CONTINUE
237      REWIND '33
238      READ('33,81) NPARTS,K,WIDTH,HEIGHT,TIME,CF
239      DO 6 N=1,NPARTS
240      READ('33,9) X(N),Y(N),VX(N),VY(N)
241      6 CONTINUE
242      IF(CF.EQ.0) CF=1
243
244      9 FORMAT(4E15,7)
245      80 FORMAT(20A3)
246      81 FORMAT(2I7,3E15,7,I1)
247
248      RETURN
249      ENDS
EOF.,
```

APPENDIX II

EXACT POSITIONS AND VELOCITIES OF  
PARTICLES OF FIGURE 1.

| X         | Y         | VX         | VY         |
|-----------|-----------|------------|------------|
| .5580E+01 | .1035E-05 | .7760E+00  | -.9628E+00 |
| .1010E+01 | .1089E-05 | .0000E+01  | .8909E-02  |
| .6848E+01 | .1808E-05 | .0000E+01  | .8909E-02  |
| .1264E+01 | .3705E-05 | .0000E+01  | .8909E-02  |
| .4311E+01 | .3991E-05 | -.6929E-06 | .8909E-02  |
| .8873E+01 | .4074E-05 | -.6649E-02 | -.1488E+00 |
| .3292E+01 | .4636E-05 | -.6834E-08 | .8909E-02  |
| .7863E+01 | .5232E-05 | .7404E-06  | -.8019E-01 |
| .1517E+01 | .5390E-05 | .0000E+01  | .8909E-02  |
| .6087E+01 | .5643E-05 | .4332E-01  | -.1856E+01 |
| .8115E+01 | .5679E-05 | .6268E-09  | .8910E-02  |
| .1000E+02 | .6378E-05 | .2528E-07  | .9277E-02  |
| .2533E+01 | .6741E-05 | .0000E+01  | -.8018E-01 |
| .4564E+01 | .7103E-05 | -.7046E-08 | .8909E-02  |
| .1772E+01 | .7293E-05 | -.6760E-07 | .8911E-02  |
| .7576E+00 | .7557E-05 | -.6962E-04 | .8909E-02  |
| .7354E+01 | .8419E-05 | .0000E+01  | .8909E-02  |
| .7610E+01 | .8523E-05 | .7481E-04  | -.8087E-01 |
| .3040E+01 | .1534E-04 | -.6103E-04 | .1714E-01  |
| .8621E+01 | .1845E-04 | -.6795E-07 | -.7127E-01 |
| .5045E+00 | .3566E-04 | -.6953E-02 | .4811E-01  |
| .3545E+01 | .3679E-04 | .6876E-01  | .1120E+00  |
| .3802E+01 | .3836E-04 | .7741E-01  | -.2867E+00 |
| .2785E+01 | .4801E-04 | -.7336E-01 | -.2765E+00 |
| .2528E+00 | .4845E-04 | .7543E+00  | -.9583E+00 |
| .2276E+01 | .6236E-04 | -.6873E-01 | -.8937E-01 |
| .8369E+01 | .7939E-04 | .2620E-02  | .2056E+00  |
| .9374E+01 | .9540E-04 | -.1417E+00 | .2155E+00  |
| .7103E+01 | .9866E-04 | .7071E-01  | .1075E+00  |
| .5323E+01 | .1023E-03 | .6140E-01  | .1179E+00  |
| .4819E+01 | .1032E-03 | .7054E-01  | .1083E+00  |
| .2025E+01 | .1040E-03 | .7049E-01  | .1087E+00  |
| .6339E+01 | .1041E-03 | .3056E-03  | .7421E-02  |
| .4603E-04 | .1070E-03 | .6281E-02  | .1152E-01  |
| .4053E+01 | .1078E-03 | .6846E-01  | .1124E+00  |
| .5831E+01 | .1198E-03 | -.4897E-02 | .2061E+00  |
| .9123E+01 | .1287E-03 | -.7536E+00 | -.9652E+00 |
| .6596E+01 | .1513E-03 | .6736E-01  | -.2885E+00 |
| .9624E+01 | .1854E-03 | -.3535E-02 | .2063E+00  |
| .5072E+01 | .1923E-03 | -.1101E+01 | -.1770E+00 |
| .9755E+01 | .2114E+00 | -.2804E+01 | -.6026E-01 |
| .5959E+01 | .2136E+00 | -.1293E+02 | .3520E+01  |
| .1644E+01 | .2147E+00 | .7979E+00  | -.8681E+01 |
| .4693E+01 | .2148E+00 | .1621E+01  | -.3314E+01 |
| .1900E+01 | .2148E+00 | -.6191E+01 | -.4237E+01 |
| .8244E+01 | .2149E+00 | .1826E+01  | -.1290E+01 |
| .9499E+01 | .2151E+00 | .2594E+01  | .3085E+00  |
| .6977E+01 | .2154E+00 | -.1016E+01 | .4487E+01  |
| .1262E+00 | .2156E+00 | -.8578E+00 | -.4029E+00 |
| .5453E+01 | .2157E+00 | -.3167E+01 | .4342E+01  |
| .1136E+01 | .2160E+00 | -.2693E+01 | -.3435E+01 |
| .2403E+01 | .2161E+00 | .8476E+01  | -.2016E+01 |
| .9247E+01 | .2164E+00 | .4353E+01  | -.1215E+01 |
| .8854E+00 | .2169E+00 | .4936E+01  | -.1517E+00 |
| .8493E+01 | .2172E+00 | -.1270E+01 | .2033E+01  |
| .6465E+01 | .2175E+00 | -.7811E+00 | .7099E+01  |
| .4440E+01 | .2177E+00 | .3445E+01  | -.1536E+01 |

| x         | y         | vx         | vy         |
|-----------|-----------|------------|------------|
| .3428E+01 | .2177E+00 | .1060E+02  | .3785E+01  |
| .6333E+00 | .2177E+00 | .3374E+01  | -.6543E+00 |
| .6212E+01 | .2180E+00 | .2114E+01  | .1053E+02  |
| .7988E+01 | .2180E+00 | -.3930E+01 | -.2622E+01 |
| .8997E+01 | .2182E+00 | -.6117E+00 | -.6517E+00 |
| .5203E+01 | .2182E+00 | .2260E+01  | -.5672E+01 |
| .3780E+00 | .2182E+00 | .2503E+01  | .3725E+01  |
| .3935E+01 | .2184E+00 | .3353E+01  | .2612E+01  |
| .5712E+01 | .2189E+00 | -.9197E+00 | -.1931E+00 |
| .7484E+01 | .2189E+00 | -.3995E+01 | -.1031E+01 |
| .2908E+01 | .2192E+00 | .1943E+01  | .2967E+00  |
| .6721E+01 | .2193E+00 | .3761E+00  | .3233E+01  |
| .4183E+01 | .2194E+00 | -.2525E+01 | -.2385E+00 |
| .2653E+01 | .2196E+00 | -.7430E+01 | -.3101E+01 |
| .3676E+01 | .2197E+00 | .3504E+01  | .7239E+01  |
| .4945E+01 | .2201E+00 | -.5614E+01 | .7176E+01  |
| .2150E+01 | .2205E+00 | .1531E+01  | .2447E+01  |
| .3159E+01 | .2209E+00 | -.5137E+01 | .3167E+00  |
| .7741E+01 | .2213E+00 | .3554E+01  | -.4987E+01 |
| .1389E+01 | .2223E+00 | -.5029E+01 | -.3864E+01 |
| .8745E+01 | .2258E+00 | .2411E+01  | .1223E+00  |
| .7229E+01 | .2279E+00 | .3490E+01  | -.8590E+00 |
| .1000E+02 | .2503E+00 | -.1154E+00 | .1154E-01  |
| .9638E+01 | .4249E+00 | .7596E+01  | -.4983E+01 |
| .4566E+01 | .4310E+00 | -.5307E+00 | .2875E+01  |
| .4293E-04 | .4313E+00 | .1134E+00  | -.1273E-01 |
| .2020E+01 | .4316E+00 | .2939E+01  | -.2282E+01 |
| .2513E+00 | .4324E+00 | .7893E+00  | -.5008E+01 |
| .4055E+01 | .4327E+00 | -.2715E+00 | -.8475E+01 |
| .1520E+01 | .4328E+00 | .1505E+01  | -.3524E+01 |
| .3289E+01 | .4339E+00 | -.2228E+01 | -.6618E+01 |
| .5577E+01 | .4341E+00 | -.2840E+01 | -.7792E+01 |
| .1002E+01 | .4345E+00 | -.3360E+01 | -.8284E+01 |
| .4818E+01 | .4351E+00 | .3080E+01  | .3326E+01  |
| .2278E+01 | .4353E+00 | .2907E+01  | -.5644E+01 |
| .3551E+01 | .4355E+00 | .7534E+01  | -.8890E+01 |
| .6596E+01 | .4357E+00 | -.1279E+00 | .4241E-01  |
| .5327E+01 | .4360E+00 | .6322E+01  | -.8165E+00 |
| .5839E+01 | .4362E+00 | -.1213E+01 | -.3767E+01 |
| .5021E+00 | .4363E+00 | .4611E+01  | .1039E+01  |
| .5071E+01 | .4364E+00 | .3345E+00  | .2862E+01  |
| .7538E+00 | .4366E+00 | .6286E+01  | .1293E+01  |
| .8370E+01 | .4372E+00 | -.2119E+01 | -.2276E+01 |
| .8875E+01 | .4376E+00 | .1970E+01  | -.1221E+01 |
| .6340E+01 | .4377E+00 | .4496E+01  | .2139E+00  |
| .9129E+01 | .4378E+00 | .3420E+01  | -.6651E+00 |
| .2533E+01 | .4392E+00 | .6284E+01  | .4897E+01  |
| .9385E+01 | .4392E+00 | -.6228E+01 | .6604E+00  |
| .6850E+01 | .4393E+00 | -.7286E+00 | .5108E+01  |
| .1261E+01 | .4394E+00 | .3239E+01  | .1203E-01  |
| .6092E+01 | .4399E+00 | -.2846E+01 | .8716E+01  |
| .3803E+01 | .4399E+00 | -.2460E+00 | -.5323E-03 |
| .7609E+01 | .4412E+00 | -.7220E+01 | .8054E+01  |
| .1770E+01 | .4415E+00 | .3802E+01  | .5375E+01  |
| .4309E+01 | .4420E+00 | .2690E+01  | .9516E+00  |
| .3045E+01 | .4427E+00 | -.1014E+02 | -.7890E+01 |
| .7860E+01 | .4432E+00 | .2802E+01  | -.5128E+01 |

| X         | Y         | VX         | VY         |
|-----------|-----------|------------|------------|
| .2796E+01 | .4435E+00 | .4161E+01  | .1609E+01  |
| .7108E+01 | .4449E+00 | .9338E+01  | -.8832E+01 |
| .8625E+01 | .4458E+00 | .8396E+01  | -.8907E+00 |
| .8112E+01 | .4470E+00 | -.1993E+01 | .7933E+01  |
| .7360E+01 | .4539E+00 | -.1464E+01 | -.1263E+01 |
| .9997E+01 | .5001E+00 | -.6774E+00 | -.4066E+01 |
| .9774E+01 | .6383E+00 | -.4695E+01 | .2357E+01  |
| .3419E+01 | .6476E+00 | -.7239E+01 | .8553E+00  |
| .1241E+00 | .6478E+00 | .1463E+01  | -.1224E+01 |
| .9523E+01 | .6494E+00 | -.4834E+01 | -.6574E+01 |
| .3734E+00 | .6503E+00 | .6271E-01  | -.2044E+01 |
| .2147E+01 | .6518E+00 | -.6971E+01 | .3954E+01  |
| .4693E+01 | .6524E+00 | .2269E+01  | .8792E+01  |
| .1125E+01 | .6531E+00 | -.1020E+01 | .1692E+01  |
| .6723E+01 | .6534E+00 | -.7646E+01 | -.1864E+01 |
| .5204E+01 | .6535E+00 | -.2077E+01 | -.8840E+01 |
| .5710E+01 | .6550E+00 | -.1338E+01 | .4234E+00  |
| .4437E+01 | .6554E+00 | -.1096E+02 | -.5132E+01 |
| .8734E+00 | .6558E+00 | -.1180E+02 | .3076E+00  |
| .6243E+00 | .6560E+00 | .6732E+00  | .2202E+01  |
| .2408E+01 | .6562E+00 | -.1298E+01 | .3177E+00  |
| .2664E+01 | .6569E+00 | .3915E+01  | .1055E+02  |
| .6232E+01 | .6573E+00 | .5476E+00  | -.8019E+01 |
| .1642E+01 | .6575E+00 | -.4641E+00 | .1706E+01  |
| .6477E+01 | .6577E+00 | -.9123E+01 | -.2776E-01 |
| .4945E+01 | .6577E+00 | .1526E+01  | -.1027E+02 |
| .5454E+01 | .6583E+00 | -.4101E+01 | .7464E+01  |
| .8751E+01 | .6593E+00 | .8352E+01  | -.3758E+01 |
| .9010E+01 | .6603E+00 | -.2892E+01 | .6644E+01  |
| .3174E+01 | .6616E+00 | -.7208E+01 | -.7296E+01 |
| .5962E+01 | .6616E+00 | -.3039E+01 | -.7491E+01 |
| .6983E+01 | .6631E+00 | .7114E+01  | .1020E+02  |
| .3919E+01 | .6633E+00 | -.4973E+01 | -.4570E+01 |
| .8247E+01 | .6639E+00 | -.6844E+00 | .4048E+01  |
| .1380E+01 | .6642E+00 | -.1886E+01 | -.4436E+01 |
| .3666E+01 | .6647E+00 | .2063E+01  | -.2052E+00 |
| .7749E+01 | .6649E+00 | .5740E+01  | .4830E+01  |
| .1891E+01 | .6661E+00 | -.3587E+01 | .2480E+01  |
| .7498E+01 | .6667E+00 | -.3923E+01 | .1417E+01  |
| .7239E+01 | .6693E+00 | .1471E+02  | -.1769E+01 |
| .8499E+01 | .6714E+00 | .3116E+01  | .6744E+01  |
| .9268E+01 | .6720E+00 | -.1383E+01 | .2611E+01  |
| .8001E+01 | .6771E+00 | -.3148E+01 | -.1925E+01 |
| .2922E+01 | .6783E+00 | -.7270E+01 | .5765E+00  |
| .4172E+01 | .6788E+00 | -.1571E+02 | -.2152E+01 |
| .1000E+02 | .7511E+00 | -.4643E-01 | .1743E+01  |
| .1977E-03 | .8638E+00 | .2292E+00  | -.1279E-01 |
| .2478E+00 | .8675E+00 | .3088E+01  | .2221E+01  |
| .5077E+01 | .8705E+00 | -.1978E+01 | .8680E+00  |
| .4567E+01 | .8723E+00 | .9426E+00  | .8749E+01  |
| .7499E+00 | .8724E+00 | .4378E+01  | .3740E+01  |
| .2276E+01 | .8726E+00 | -.6290E+00 | .5943E+01  |
| .9981E+00 | .8731E+00 | -.2942E+01 | .2638E+01  |
| .5008E+00 | .8739E+00 | .1965E+01  | -.3726E+00 |
| .6601E+01 | .8745E+00 | -.1727E+01 | -.4611E+01 |
| .9683E+01 | .8746E+00 | -.2557E+00 | -.4271E+01 |
| .4817E+01 | .8747E+00 | .1202E+02  | .2152E+00  |

| X         | Y         | VX         | VY         |
|-----------|-----------|------------|------------|
| .5582E+01 | .8754E+00 | .5282E+01  | -.3232E+01 |
| .5324E+01 | .8762E+00 | -.1078E+02 | -.3021E+01 |
| .2782E+01 | .8800E+00 | .2247E+01  | -.2528E+01 |
| .6086E+01 | .8811E+00 | .1308E+01  | -.7149E+01 |
| .2525E+01 | .8820E+00 | -.2855E+01 | -.2607E+01 |
| .1508E+01 | .8822E+00 | .1994E+01  | .8953E+00  |
| .3286E+01 | .8823E+00 | -.3710E+01 | .1334E+01  |
| .9140E+01 | .8839E+00 | .4264E+01  | -.8254E+01 |
| .7365E+01 | .8840E+00 | -.5459E+01 | -.5534E+01 |
| .8363E+01 | .8856E+00 | -.8493E+00 | .2520E+01  |
| .1258E+01 | .8856E+00 | .3427E+01  | -.3919E+01 |
| .4326E+01 | .8859E+00 | .3689E+01  | .3573E+01  |
| .2027E+01 | .8861E+00 | .5186E+01  | -.3873E+01 |
| .5835E+01 | .8866E+00 | .2303E+00  | .4574E+01  |
| .8891E+01 | .8888E+00 | -.1490E+01 | .1169E+02  |
| .1758E+01 | .8893E+00 | -.6995E+01 | .3153E+01  |
| .7614E+01 | .8913E+00 | -.3382E+01 | .9474E+00  |
| .3545E+01 | .8926E+00 | -.7152E+00 | .5870E+01  |
| .9401E+01 | .8927E+00 | -.6216E+01 | -.3465E+01 |
| .7866E+01 | .8935E+00 | -.5198E+01 | .1398E+01  |
| .7112E+01 | .8954E+00 | .2002E+01  | .2081E+01  |
| .8117E+01 | .9003E+00 | .4254E+01  | .1587E+01  |
| .4064E+01 | .9040E+00 | -.1179E+01 | .1008E+02  |
| .3035E+01 | .9053E+00 | .4181E+01  | .9615E+01  |
| .8619E+01 | .9061E+00 | .7801E+01  | .6855E+01  |
| .3808E+01 | .9087E+00 | -.1831E+01 | -.1946E+01 |
| .6346E+01 | .9105E+00 | -.7049E+00 | .2873E+01  |
| .6855E+01 | .9121E+00 | .5624E+00  | .1238E+02  |
| .1000E+02 | .1001E+01 | -.8855E-01 | -.4587E+00 |
| .1202E+00 | .1083E+01 | -.1068E+01 | .3771E+01  |
| .5202E+01 | .1090E+01 | -.1753E+01 | -.8044E+01 |
| .2658E+01 | .1091E+01 | .4015E+01  | -.3096E+01 |
| .8724E+00 | .1091E+01 | -.4509E+01 | -.3843E+01 |
| .5694E+01 | .1093E+01 | -.7343E+01 | -.6982E+00 |
| .3699E+00 | .1093E+01 | .2651E+01  | -.5454E+01 |
| .2405E+01 | .1099E+01 | -.5002E+01 | -.4924E+01 |
| .1116E+01 | .1099E+01 | -.1047E+01 | -.1081E+01 |
| .4687E+01 | .1100E+01 | .4771E-01  | -.1019E+02 |
| .4952E+01 | .1101E+01 | .3438E+01  | .5935E+01  |
| .1630E+01 | .1102E+01 | .8767E-01  | -.7490E+01 |
| .6232E+00 | .1102E+01 | .3486E+01  | -.1304E+01 |
| .1376E+01 | .1105E+01 | .3812E+01  | .3136E+00  |
| .9287E+01 | .1105E+01 | .4525E+01  | -.8745E+01 |
| .9017E+01 | .1106E+01 | .4265E+01  | -.1086E+02 |
| .6698E+01 | .1106E+01 | -.2197E-01 | .6717E+01  |
| .7991E+01 | .1110E+01 | .6768E+01  | -.3679E+01 |
| .9538E+01 | .1111E+01 | .4360E+00  | -.3245E+01 |
| .2155E+01 | .1112E+01 | .2480E+01  | -.4892E+01 |
| .6200E+01 | .1112E+01 | .4369E+01  | -.8783E+00 |
| .3164E+01 | .1116E+01 | -.9527E+01 | -.3158E+01 |
| .5946E+01 | .1116E+01 | .4165E+01  | -.7175E+01 |
| .7226E+01 | .1116E+01 | -.2917E+01 | -.6427E+01 |
| .1907E+01 | .1116E+01 | .1923E+01  | -.8450E+00 |
| .3674E+01 | .1120E+01 | .3990E+01  | -.1182E+01 |
| .8491E+01 | .1122E+01 | .2010E-01  | -.1128E+01 |
| .4433E+01 | .1122E+01 | -.6286E+01 | .3509E+01  |
| .2906E+01 | .1124E+01 | .3399E+01  | -.2024E+01 |
| .4179E+01 | .1128E+01 | -.1166E+02 | -.1319E+01 |

| X         | Y         | VX         | VY         |
|-----------|-----------|------------|------------|
| .9785E+01 | .1132E+01 | -.4160E+01 | -.3916E+01 |
| .3931E+01 | .1136E+01 | -.2895E+01 | .7365E+01  |
| .7747E+01 | .1138E+01 | -.6630E+01 | -.4946E+01 |
| .3406E+01 | .1138E+01 | .1061E+01  | -.3618E+00 |
| .7483E+01 | .1140E+01 | -.2701E+01 | .3468E+00  |
| .8753E+01 | .1142E+01 | .4470E+01  | .9234E+01  |
| .5440E+01 | .1148E+01 | -.9296E+01 | -.7206E+01 |
| .8241E+01 | .1154E+01 | -.2885E+01 | -.1293E+02 |
| .6449E+01 | .1156E+01 | .2334E+01  | -.3654E+01 |
| .6979E+01 | .1172E+01 | .5354E+01  | -.1394E+01 |
| .1000E+02 | .1252E+01 | .9579E+00  | .6707E+00  |
| .2511E-04 | .1299E+01 | .6013E-01  | -.9834E-02 |
| .2509E+00 | .1318E+01 | -.4326E+01 | -.1484E+01 |
| .1773E+01 | .1329E+01 | .6521E+01  | -.3808E+01 |
| .1519E+01 | .1333E+01 | .1481E+01  | -.9733E+01 |
| .5263E+01 | .1336E+01 | .1607E+01  | -.1608E+01 |
| .9149E+01 | .1341E+01 | -.4420E+00 | .2247E+01  |
| .7835E+00 | .1342E+01 | .1490E+01  | .2522E+01  |
| .1259E+01 | .1344E+01 | .3413E+01  | -.1026E+01 |
| .5320E+00 | .1345E+01 | .2889E+00  | -.1019E+00 |
| .4885E+01 | .1351E+01 | .5436E+00  | -.1307E+02 |
| .3557E+01 | .1353E+01 | -.9324E+01 | .1171E+01  |
| .3267E+01 | .1356E+01 | .3056E+01  | .4603E+01  |
| .4614E+01 | .1357E+01 | -.3406E+01 | -.8006E+01 |
| .2438E+01 | .1358E+01 | .3944E+01  | -.6204E+01 |
| .3815E+01 | .1358E+01 | -.2846E+01 | .4815E+01  |
| .8885E+01 | .1364E+01 | -.3547E+01 | .2977E+01  |
| .7208E+01 | .1368E+01 | -.1506E+01 | -.1061E+02 |
| .2697E+01 | .1370E+01 | -.9083E+01 | -.1227E+01 |
| .2030E+01 | .1371E+01 | -.4534E+01 | -.6666E+01 |
| .6710E+01 | .1376E+01 | .5037E+01  | -.1346E+02 |
| .9757E+01 | .1378E+01 | -.8266E+00 | .9666E+00  |
| .4079E+01 | .1379E+01 | .4498E+01  | .6053E+01  |
| .6170E+01 | .1385E+01 | -.3666E+01 | .6173E+01  |
| .5786E+01 | .1389E+01 | -.3249E+01 | -.2861E+01 |
| .7989E+01 | .1390E+01 | -.3804E+01 | -.2275E+01 |
| .8598E+01 | .1399E+01 | -.4892E+01 | .5438E+00  |
| .7739E+01 | .1403E+01 | -.2093E+01 | -.5695E+00 |
| .4360E+01 | .1405E+01 | .3262E+01  | -.1640E+01 |
| .8250E+01 | .1411E+01 | -.8392E+01 | -.1317E+02 |
| .6423E+01 | .1415E+01 | .6396E+01  | .1647E+01  |
| .9472E+01 | .1415E+01 | .4491E+01  | .9245E+01  |
| .7460E+01 | .1423E+01 | -.8406E+01 | .4747E+01  |
| .1019E+01 | .1424E+01 | .4809E+01  | -.1925E+01 |
| .2970E+01 | .1428E+01 | .4182E+01  | .5066E+01  |
| .5493E+01 | .1430E+01 | .4813E+01  | .8445E+01  |
| .9999E+01 | .1503E+01 | -.1193E+00 | .1065E+01  |
| .6977E+01 | .1514E+01 | .8306E+01  | -.5457E+01 |
| .6765E-02 | .1549E+01 | .8169E+00  | .1509E+01  |

APPENDIX III

EXACT POSITIONS AND VELOCITIES OF  
FLUID #4 IN TABLE II

| X         | Y         | VX         | VY         |
|-----------|-----------|------------|------------|
| .0000E+01 | .5797E+01 | .1078E+00  | .8583E-02  |
| .2777E+01 | .5116E+01 | -.2990E+00 | .7128E+00  |
| .3336E+01 | .5297E+01 | -.1939E+00 | .2060E+01  |
| .4503E+01 | .3587E+01 | -.4623E+00 | .1722E-01  |
| .3293E+01 | .0000E+01 | .7153E-03  | .2951E+00  |
| .1243E+01 | .6280E+01 | .1819E+00  | .6555E+00  |
| .0000E+01 | .1493E+01 | .2729E+00  | .2384E-02  |
| .1905E+01 | .3260E+01 | -.5983E-01 | .2715E+00  |
| .3685E+01 | .0000E+01 | -.4292E-02 | .2947E+00  |
| .5155E+01 | .8196E+01 | -.8128E+00 | .1620E+01  |
| .1821E+00 | .0000E+01 | .1192E-03  | .5636E+00  |
| .6000E+01 | .2510E+01 | -.2189E+00 | .4768E-02  |
| .6000E+01 | .3050E+01 | -.1984E+00 | .5960E-02  |
| .3082E+01 | .2188E+01 | -.3898E-01 | .2469E+00  |
| .4662E+01 | .0000E+01 | .0000E+01  | .3082E+00  |
| .4322E+01 | .4707E+00 | .1887E+00  | .9281E-01  |
| .4535E+01 | .3085E+01 | -.6691E-01 | .1354E+00  |
| .5817E+01 | .0000E+01 | .4768E-03  | .5705E+00  |
| .0000E+01 | .2506E+00 | .5609E+00  | .9239E-03  |
| .0000E+01 | .2280E+01 | .2322E+00  | .3576E-02  |
| .2509E+01 | .0000E+01 | .0000E+01  | .2971E+00  |
| .3784E+01 | .4287E+01 | -.2607E+00 | .1131E+01  |
| .1630E+01 | .4847E+00 | .2387E-01  | .3357E-01  |
| .2901E+01 | .0000E+01 | -.2384E-03 | .2960E+00  |
| .9304E+00 | .8689E+01 | -.3379E+00 | .1914E+01  |
| .3557E+01 | .6054E+01 | .2987E+00  | .6208E-01  |
| .2734E+01 | .8897E+00 | .2476E+00  | -.3001E-02 |
| .1922E+01 | .0000E+01 | -.3576E-03 | .2974E+00  |
| .5628E+01 | .0000E+01 | .0000E+01  | .3938E+00  |
| .5166E+01 | .1420E+01 | .1545E-01  | .2001E+00  |
| .2221E+01 | .1788E+01 | .1619E+00  | -.5859E-01 |
| .2583E+01 | .2105E+01 | -.3888E-01 | .2214E+00  |
| .4701E+01 | .1638E+01 | -.7210E-01 | .2498E+00  |
| .2521E+01 | .4872E+00 | .2012E+00  | .1201E-01  |
| .6000E+01 | .8578E+01 | -.4005E-01 | .1049E-01  |
| .6000E+01 | .1726E+01 | -.2642E+00 | .3099E-02  |
| .6000E+01 | .3605E+01 | -.1764E+00 | .6914E-02  |
| .6000E+01 | .1050E+02 | -.9060E-02 | .2861E-02  |
| .1330E+01 | .2001E+01 | .2444E+00  | .1867E+00  |
| .3983E+01 | .3224E+01 | -.2535E+00 | .1120E+01  |
| .5392E+01 | .5373E+01 | -.9982E-01 | .8247E+00  |
| .3553E+01 | .8963E+01 | -.5288E+00 | .2075E+01  |
| .2108E+01 | .4354E+01 | -.4406E+00 | .2704E+00  |
| .5456E+01 | .3684E+01 | -.9003E-01 | .2872E+00  |
| .5075E+01 | .2367E+01 | -.4963E-01 | .2482E+00  |
| .3157E+01 | .4152E+01 | .3992E+00  | .9712E+00  |
| .6000E+01 | .3889E+01 | -.1636E+00 | .7153E-02  |
| .6456E+00 | .5934E+01 | -.6146E-01 | .1218E+01  |
| .4428E+01 | .9731E+01 | .4942E+00  | .3190E+01  |
| .2504E+01 | .1327E+01 | .2576E+00  | -.3795E-02 |
| .0000E+01 | .3664E+01 | .1795E+00  | .5960E-02  |
| .3501E+01 | .6749E+01 | .4603E+00  | .5283E+00  |
| .2053E+01 | .1314E+01 | .2047E+00  | -.4431E-01 |
| .5247E+01 | .7424E+01 | -.4783E+00 | .2303E+01  |
| .6000E+01 | .1984E+01 | -.2441E+00 | .3695E-02  |
| .1407E+01 | .3042E+01 | .3020E-01  | .1610E+00  |
| .5114E+01 | .8948E+00 | -.3745E-01 | .5905E-01  |

|           |           |            |           |
|-----------|-----------|------------|-----------|
| .1825E+01 | .2723E+01 | .7638E-01  | .2244E+00 |
| .5051E+01 | .0000E+01 | .0000E+01  | .3218E+00 |
| .7547E+00 | .0000E+01 | .5364E-03  | .3301E+00 |
| .1880E+01 | .6588E+01 | -.2454E-01 | .8165E+00 |
| .0000E+01 | .9691E+01 | .2000E-01  | .5722E-02 |
| .0000E+01 | .2014E+01 | .2470E+00  | .3099E-02 |
| .4674E+01 | .7012E+01 | -.6573E-01 | .1167E+01 |
| .4089E+01 | .2220E+01 | -.2322E-02 | .5702E+00 |
| .4630E+01 | .2568E+01 | -.2295E+00 | .1546E+00 |
| .0000E+01 | .4246E+01 | .1579E+00  | .6676E-02 |
| .6000E+01 | .9959E+01 | -.1431E-01 | .5722E-02 |
| .7717E+00 | .7948E+01 | .3193E+00  | .1189E+01 |
| .6000E+01 | .7256E+00 | -.3214E+00 | .1490E-02 |
| .5623E+00 | .0000E+01 | .5364E-03  | .3487E+00 |
| .6000E+01 | .8169E+01 | -.4911E-01 | .1049E-01 |
| .3881E+01 | .0000E+01 | -.2384E-03 | .3036E+00 |
| .1470E+01 | .3584E+01 | -.2523E+00 | .2028E+00 |
| .3754E+01 | .8019E+01 | -.4994E+00 | .1163E+01 |
| .6000E+01 | .6691E+01 | -.8583E-01 | .1049E-01 |
| .4172E+01 | .2708E+01 | -.2576E+00 | .7443E+00 |
| .3583E+01 | .2237E+01 | .2572E-01  | .4870E+00 |
| .7289E+00 | .7242E+01 | .3425E+00  | .1478E+01 |
| .0000E+01 | .1752E+01 | .2618E+00  | .2623E-02 |
| .4948E+01 | .3920E+01 | -.1302E+00 | .1381E+00 |
| .0000E+01 | .8341E+01 | .4741E-01  | .9537E-02 |
| .4225E+01 | .1744E+01 | -.1532E+00 | .4209E+00 |
| .2974E+01 | .6410E+01 | .3214E+00  | .1386E+01 |
| .2785E+01 | .1702E+01 | .4907E-01  | .1357E+00 |
| .0000E+01 | .3952E+01 | .1634E+00  | .6676E-02 |
| .5517E+01 | .2171E+01 | -.2545E-01 | .2247E+00 |
| .6000E+01 | .4846E+00 | -.3772E+00 | .1073E-02 |
| .4076E+01 | .0000E+01 | .3815E-02  | .2989E+00 |
| .1599E+01 | .1241E+01 | .5048E-01  | .1599E+00 |
| .4911E+01 | .4457E+01 | .3357E-01  | .3823E+00 |
| .6000E+01 | .1219E+01 | -.2937E+00 | .1788E-02 |
| .4518E+00 | .8363E+00 | .9769E-01  | .2386E-01 |
| .5318E+01 | .6712E+01 | .3959E-01  | .2001E+01 |
| .8901E+00 | .1311E+01 | .5891E-01  | .1651E+00 |
| .5533E+00 | .4182E+01 | -.1067E+00 | .6131E+00 |
| .4396E+01 | .4141E+01 | .5286E+00  | .4442E+00 |
| .4594E+01 | .2099E+01 | -.4083E-01 | .2057E+00 |
| .9480E+00 | .0000E+01 | .2980E-03  | .3159E+00 |
| .1015E+01 | .3891E+01 | -.2658E+00 | .1641E+00 |
| .0000E+01 | .1237E+01 | .2915E+00  | .1907E-02 |
| .5417E+01 | .4773E+01 | .1369E+00  | .4334E+00 |
| .0000E+01 | .3379E+01 | .1835E+00  | .5484E-02 |
| .2696E+01 | .4540E+01 | -.2631E+00 | .4703E+00 |
| .4007E+01 | .3755E+01 | -.1247E+00 | .1592E+01 |
| .3752E+01 | .1778E+01 | -.9517E-01 | .3680E+00 |
| .9182E+00 | .2304E+01 | .6367E-01  | .1270E+00 |
| .3097E+01 | .0000E+01 | .2384E-03  | .2941E+00 |
| .5437E+01 | .0000E+01 | .4768E-03  | .3460E+00 |
| .1764E+01 | .5909E+01 | .2921E+00  | .7587E+00 |
| .2117E+01 | .0000E+01 | -.4768E-03 | .3005E+00 |
| .5184E+01 | .4799E+00 | -.3975E-01 | .2413E-01 |
| .8132E+00 | .4726E+00 | .1019E+00  | .5680E-01 |
| .1726E+01 | .0000E+01 | -.3576E-03 | .3000E+00 |

|           |           |            |            |
|-----------|-----------|------------|------------|
| .0000E+01 | .1080E+02 | .7311E-02  | -.9537E-03 |
| .1941E+01 | .7307E+01 | -.5661E+00 | .1164E+01  |
| .0000E+01 | .6816E+01 | .8196E-01  | .9537E-02  |
| .2209E+01 | .2391E+01 | .2083E+00  | .5102E+00  |
| .4549E+01 | .7769E+01 | -.1289E+01 | .1478E+01  |
| .0000E+01 | .7365E+00 | .3265E+00  | .1371E-02  |
| .3910E+01 | .1319E+01 | .7618E-01  | .3039E+00  |
| .4000E+01 | .7289E+01 | -.3216E+00 | .9837E+00  |
| .2305E+01 | .5534E+01 | -.2111E-01 | .5833E+00  |
| .6000E+01 | .6019E+01 | -.1044E+00 | .1001E-01  |
| .6000E+01 | .0000E+01 | -.2174E+00 | .1043E+00  |
| .3214E+01 | .2683E+01 | -.1087E+00 | .2874E+00  |
| .2437E+01 | .3448E+01 | -.8363E-01 | .7102E+00  |
| .3293E+01 | .4688E+01 | -.6489E+00 | .1581E+01  |
| .1066E+01 | .4448E+01 | -.3658E+00 | .3953E+00  |
| .3489E+01 | .0000E+01 | .0000E+01  | .2991E+00  |
| .0000E+01 | .1149E+02 | .4224E-02  | -.8583E-02 |
| .6793E+00 | .6568E+01 | .2371E+00  | .1364E+01  |
| .0000E+01 | .6467E+01 | .9141E-01  | .9060E-02  |
| .0000E+01 | .6128E+01 | .9906E-01  | .9060E-02  |
| .1701E+01 | .5288E+01 | .5096E-01  | .7559E+00  |
| .4468E+01 | .0000E+01 | -.9537E-03 | .3054E+00  |
| .2077E+01 | .4815E+00 | .7390E-01  | .8792E-01  |
| .0000E+01 | .7176E+01 | .7466E-01  | .9537E-02  |
| .1818E+01 | .8630E+00 | .7528E-01  | .1099E+00  |
| .9451E+00 | .2813E+01 | .8043E-01  | .1525E-01  |
| .3016E+01 | .8255E+01 | .2940E+00  | .9810E+00  |
| .9723E+00 | .3346E+01 | -.9985E-01 | .6507E-02  |
| .5816E+00 | .4745E+01 | .3847E-01  | .9339E+00  |
| .3334E+01 | .9905E+01 | -.3491E+00 | .2017E+01  |
| .1315E+01 | .6969E+01 | .5477E-01  | .9216E+00  |
| .5244E+01 | .0000E+01 | .4768E-03  | .3234E+00  |
| .6000E+01 | .1112E+02 | -.5722E-02 | -.9537E-03 |
| .5365E+01 | .6020E+01 | -.2975E-01 | .1132E+01  |
| .5297E+00 | .3636E+01 | -.3262E-01 | .3414E+00  |
| .0000E+01 | .2549E+01 | .2232E+00  | .4053E-02  |
| .4282E+01 | .5955E+01 | .1269E+00  | .1202E+01  |
| .6000E+01 | .9467E+01 | -.2289E-01 | .7629E-02  |
| .0000E+01 | .1244E+02 | .2350E-02  | -.2289E-01 |
| .0000E+01 | .4919E+00 | .3803E+00  | .1252E-02  |
| .0000E+01 | .9212E+01 | .2748E-01  | .7629E-02  |
| .2992E+01 | .1286E+01 | .1843E+00  | .2755E-01  |
| .0000E+01 | .3099E+01 | .2008E+00  | .5007E-02  |
| .5550E+01 | .1247E+01 | -.3680E-01 | .9363E-01  |
| .4860E+01 | .5665E+01 | -.7254E-01 | .9112E+00  |
| .0000E+01 | .7549E+01 | .6578E-01  | .9537E-02  |
| .0000E+01 | .9849E+00 | .3017E+00  | .1431E-02  |
| .4901E+01 | .5026E+01 | .3903E+00  | .2597E+00  |
| .3874E+01 | .4820E+00 | .2435E+00  | .2265E+00  |
| .0000E+01 | .2822E+01 | .2059E+00  | .4530E-02  |
| .3712E+00 | .0000E+01 | .4172E-03  | .3960E+00  |
| .6000E+01 | .6351E+01 | -.9155E-01 | .1097E-01  |
| .2567E+01 | .3992E+01 | -.1258E+00 | .6990E+00  |
| .4360E+01 | .1277E+01 | .6922E-01  | .3205E+00  |
| .5118E+00 | .3107E+01 | .1430E-01  | .1699E+00  |
| .5498E+01 | .2657E+01 | -.2572E-01 | .2899E+00  |
| .8836E+00 | .8866E+00 | .1564E+00  | .1295E+00  |

|           |           |            |            |
|-----------|-----------|------------|------------|
| .5583E+01 | .4498E+00 | -.2381E-01 | .4782E-01  |
| .1545E+01 | .4133E+01 | -.4627E+00 | .3710E+00  |
| .4954E+00 | .2602E+01 | .2037E-01  | .1455E+00  |
| .5021E+01 | .9028E+01 | -.7107E+00 | .1159E+01  |
| .1796E+01 | .2171E+01 | .3835E+00  | .1017E+00  |
| .4138E+00 | .4466E+00 | .9235E-01  | .2144E-01  |
| .1156E+01 | .9608E+01 | .8196E-01  | .2250E+01  |
| .6000E+01 | .5696E+01 | -.1087E+00 | .1001E-01  |
| .2197E+01 | .4923E+01 | -.3602E+00 | .2901E+00  |
| .6000E+01 | .7779E+01 | -.5674E-01 | .1144E-01  |
| .6000E+01 | .3326E+01 | -.1864E+00 | .6437E-02  |
| .5008E+01 | .3387E+01 | -.1776E+00 | .2352E+00  |
| .2980E+01 | .3604E+01 | -.1503E+00 | .9015E+00  |
| .5042E+01 | .2879E+01 | -.6970E-01 | .2028E+00  |
| .0000E+01 | .4544E+01 | .1438E+00  | .7629E-02  |
| .2931E+01 | .5759E+01 | -.2757E+00 | .1313E+01  |
| .4578E+00 | .1239E+01 | .3395E-01  | .2408E-01  |
| .4578E+01 | .8340E+00 | .1221E+00  | .1851E+00  |
| .3275E+01 | .1748E+01 | .2797E-01  | .2572E+00  |
| .3701E+01 | .2732E+01 | -.1404E+00 | .6653E+00  |
| .6090E+00 | .5327E+01 | .1214E+00  | .9704E+00  |
| .6000E+01 | .2468E+00 | -.5646E+00 | .6706E-03  |
| .4857E+01 | .0000E+01 | -.4768E-03 | .3108E+00  |
| .5092E+01 | .1897E+01 | -.1443E-01 | .2080E+00  |
| .2969E+01 | .4848E+00 | .2820E+00  | .9068E-01  |
| .1726E+01 | .8842E+01 | .4872E-01  | .1756E+01  |
| .4321E+01 | .8591E+01 | -.1219E+01 | .2005E+01  |
| .6000E+01 | .9008E+01 | -.3195E-01 | .9537E-02  |
| .6000E+01 | .7042E+01 | -.7439E-01 | .1192E-01  |
| .2005E+01 | .3802E+01 | -.3990E+00 | .3246E+00  |
| .3663E+01 | .8866E+00 | .2638E+00  | .1039E+00  |
| .4361E+01 | .4674E+01 | -.4256E+00 | .4212E+00  |
| .0000E+01 | .4848E+01 | .1369E+00  | .7629E-02  |
| .3841E+01 | .4881E+01 | -.4950E+00 | .8764E+00  |
| .3425E+01 | .4816E+00 | .2789E+00  | .7708E-01  |
| .2711E+01 | .2589E+01 | .6965E-02  | .3860E+00  |
| .0000E+01 | .8765E+01 | .3728E-01  | .8583E-02  |
| .1267E+01 | .1517E+01 | .7874E-01  | .2078E+00  |
| .6000E+01 | .4767E+01 | -.1397E+00 | .8583E-02  |
| .6000E+01 | .1471E+01 | -.2694E+00 | .2623E-02  |
| .0000E+01 | .5158E+01 | .1257E+00  | .8106E-02  |
| .1427E+01 | .7791E+01 | .6909E+00  | .2417E+01  |
| .1375E+01 | .2504E+01 | .1685E+00  | .1040E+00  |
| .6000E+01 | .7404E+01 | -.6723E-01 | .1097E-01  |
| .2608E+01 | .7617E+01 | -.4117E+00 | .9067E+00  |
| .5433E+01 | .4216E+01 | -.6118E-01 | .2834E+00  |
| .0000E+01 | .5474E+01 | .1177E+00  | .8583E-02  |
| .6000E+01 | .4469E+01 | -.1445E+00 | .8106E-02  |
| .3427E+01 | .3199E+01 | -.3060E+00 | .4341E+00  |
| .8856E+00 | .1808E+01 | .5896E-01  | .2381E+00  |
| .6000E+01 | .5380E+01 | -.1216E+00 | .9060E-02  |
| .2278E+01 | .8924E+00 | .1979E+00  | -.3694E-02 |
| .4272E+01 | .0000E+01 | -.4768E-03 | .3090E+00  |
| .2196E+01 | .9848E+01 | .7297E-01  | .2641E+01  |
| .3858E+01 | .5521E+01 | .1156E+01  | .2248E-01  |
| .2551E+01 | .6904E+01 | -.3894E+00 | .1027E+01  |
| .0000E+01 | .1021E+02 | .1276E-01  | .2861E-02  |

|           |           |            |            |
|-----------|-----------|------------|------------|
| .2705E+01 | .0000E+01 | .0000E+01  | .2922E+00  |
| .4664E+00 | .1662E+01 | .6013E-01  | .4943E-01  |
| .4380E+01 | .5273E+01 | .8462E+00  | .2600E+00  |
| .2313E+01 | .0000E+01 | -.2384E-03 | .2942E+00  |
| .4792E+00 | .2121E+01 | -.2922E-01 | .1223E+00  |
| .3506E+01 | .3726E+01 | -.7785E-01 | .3087E+00  |
| .5535E+01 | .1708E+01 | -.5992E-02 | .1467E+00  |
| .6000E+01 | .2779E+01 | -.2089E+00 | .5484E-02  |
| .4116E+01 | .8761E+00 | .2178E+00  | .1900E+00  |
| .6000E+01 | .2246E+01 | -.2356E+00 | .4053E-02  |
| .5541E+01 | .8425E+00 | -.4405E-01 | .1192E+00  |
| .0000E+01 | .7937E+01 | .5910E-01  | .9537E-02  |
| .1142E+01 | .0000E+01 | .1192E-03  | .3068E+00  |
| .1220E+01 | .4946E+00 | .3128E-01  | .8605E-01  |
| .1312E+01 | .9222E+00 | .1554E+00  | .1054E+00  |
| .1175E+01 | .5628E+01 | -.6318E-01 | .8407E+00  |
| .3205E+01 | .8749E+00 | .2622E+00  | .4922E-01  |
| .5484E+01 | .3162E+01 | -.5815E-01 | .3287E+00  |
| .4807E+01 | .1188E+01 | .6562E-01  | .2293E+00  |
| .1742E+01 | .1699E+01 | .1886E+00  | .3699E-01  |
| .6000E+01 | .4177E+01 | -.1564E+00 | .7629E-02  |
| .6000E+01 | .1192E+02 | -.3338E-02 | -.1049E-01 |
| .3257E+01 | .7377E+01 | -.4513E+00 | .5165E+00  |
| .6000E+01 | .5070E+01 | -.1264E+00 | .9060E-02  |
| .6000E+01 | .9702E+00 | -.2995E+00 | .1431E-02  |
| .1336E+01 | .0000E+01 | -.2384E-03 | .3021E+00  |
| .3455E+01 | .1311E+01 | .1059E+00  | .1087E+00  |
| .2376E+01 | .6167E+01 | .3260E+00  | .9599E+00  |
| .1916E-05 | .0000E+01 | .2201E+00  | .1008E+00  |
| .1120E+01 | .5027E+01 | .1353E+00  | .6940E+00  |
| .4779E+01 | .4762E+00 | -.7042E-02 | .5606E-01  |
| .2092E+01 | .8161E+01 | .8859E+00  | .1735E+01  |
| .4799E+01 | .6332E+01 | .4439E+00  | .1206E+01  |
| .2323E+01 | .2925E+01 | .9646E-01  | .6106E+00  |
| .2869E+01 | .3093E+01 | -.5374E-01 | .5990E+00  |
| .4129E+01 | .6567E+01 | .8558E-01  | .9549E+00  |
| .2617E+01 | .8982E+01 | -.7750E+00 | .1673E+01  |
| .1531E+01 | .0000E+01 | -.3576E-03 | .3023E+00  |
| .1617E+01 | .4698E+01 | -.3685E+00 | .4827E+00  |

APPENDIX IV

EXACT POSITIONS AND VELOCITIES  
OF FLUID #10 IN TABLE II

| X         | Y         | VX         | VY         |
|-----------|-----------|------------|------------|
| .7826E+00 | .3530E+01 | -.1224E+01 | .2475E+01  |
| .2138E+01 | .1747E+01 | -.1842E+01 | -.8631E+01 |
| .5027E+01 | .1865E+01 | -.8593E+01 | .6766E+00  |
| .5240E+01 | .4947E+01 | -.1017E+02 | .5168E+01  |
| .3286E+01 | .0000E+01 | -.4768E-02 | .3867E-01  |
| .1211E+01 | .2662E+01 | -.3027E+01 | .7531E+00  |
| .0000E+01 | .1489E+01 | .3967E-01  | .2384E-02  |
| .6578E+00 | .1891E+01 | -.3969E+01 | .6695E+01  |
| .3676E+01 | .0000E+01 | -.2384E-02 | .3966E-01  |
| .4789E+01 | .4805E+01 | .4357E+01  | .6557E+01  |
| .1868E+00 | .0000E+01 | .1043E-02  | .4422E-01  |
| .6000E+01 | .2501E+01 | -.2384E-01 | .0000E+01  |
| .6000E+01 | .3039E+01 | -.1907E-01 | -.2384E-02 |
| .1783E+01 | .9135E+00 | -.3059E+01 | -.1105E+01 |
| .4647E+01 | .0000E+01 | -.4768E-02 | .4150E-01  |
| .3908E+01 | .6327E+00 | .1817E+01  | -.4131E+01 |
| .5163E+01 | .1194E+01 | .1030E+01  | .1504E+01  |
| .5810E+01 | .0000E+01 | .0000E+01  | .5209E-01  |
| .0000E+01 | .2485E+00 | .4438E-01  | -.2980E-03 |
| .0000E+01 | .2273E+01 | .2812E-01  | -.7153E-02 |
| .2506E+01 | .0000E+01 | .0000E+01  | .3960E-01  |
| .4251E+01 | .6299E+00 | -.4442E-01 | .1134E+01  |
| .1040E+01 | .3552E+00 | -.5079E+01 | .7716E+00  |
| .2896E+01 | .0000E+01 | -.2384E-02 | .3538E-01  |
| .3514E+01 | .2413E+01 | .7775E+01  | -.5090E+01 |
| .5680E+01 | .1554E+01 | -.3078E+01 | .3598E+01  |
| .2451E+01 | .3249E+00 | -.3750E+01 | -.5737E+00 |
| .1922E+01 | .0000E+01 | .0000E+01  | .3427E-01  |
| .5616E+01 | .0000E+01 | -.4768E-02 | .4384E-01  |
| .5597E+01 | .5878E+00 | -.2885E+01 | .8567E+00  |
| .1407E+01 | .3170E+00 | -.1174E+01 | .6465E+01  |
| .1517E+01 | .1200E+01 | -.4106E+01 | -.7364E+01 |
| .3770E+01 | .3259E+00 | .1972E+01  | -.6410E+01 |
| .2534E+01 | .1217E+01 | -.3771E+01 | -.4184E+01 |
| .1460E+01 | .2387E+01 | -.6574E+01 | -.8676E+00 |
| .6000E+01 | .1721E+01 | -.3338E-01 | .0000E+01  |
| .6000E+01 | .3595E+01 | -.1907E-01 | -.2384E-02 |
| .2107E+01 | .5499E+01 | -.6795E+01 | .1845E+01  |
| .6023E+00 | .9108E+00 | .2505E+01  | .3615E+00  |
| .5249E+01 | .6410E+00 | .2225E+01  | .3740E+01  |
| .4293E+01 | .3214E+01 | -.3581E+01 | -.2580E+01 |
| .5599E+01 | .2636E+01 | -.9423E+01 | -.2795E+01 |
| .2333E+01 | .2010E+01 | -.3822E+01 | .2854E+01  |
| .5641E+01 | .1889E+01 | -.6479E+01 | -.1147E-01 |
| .5021E+01 | .1551E+01 | -.6594E+00 | -.4438E+01 |
| .1635E+01 | .2668E+01 | -.3243E+01 | .3010E+01  |
| .6000E+01 | .3883E+01 | -.1431E-01 | .0000E+01  |
| .1305E+01 | .5004E+01 | .1714E+01  | -.6307E+01 |
| .2239E+01 | .4330E+01 | -.1298E+01 | .2550E+01  |
| .2201E+01 | .1210E+01 | .3417E+00  | -.2661E+01 |
| .0000E+01 | .3647E+01 | .1484E-01  | -.2384E-02 |
| .3312E+01 | .2753E+01 | -.1282E+01 | -.5342E+01 |
| .1450E+01 | .8970E+00 | -.6718E+01 | -.3571E+01 |
| .2594E+01 | .2998E+01 | -.3186E+01 | -.4163E+01 |
| .6000E+01 | .1977E+01 | -.2861E-01 | -.2384E-02 |
| .8821E+00 | .1051E+01 | -.2973E+01 | -.3881E+01 |
| .5368E+01 | .3292E+00 | .1037E+01  | .5568E+00  |

|           |           |            |            |
|-----------|-----------|------------|------------|
| .9180E+00 | .2041E+01 | -.1059E+01 | .5578E-01  |
| .5034E+01 | .0000E+01 | -.4768E-02 | .4034E-01  |
| .7623E+00 | .0000E+01 | .2384E-02  | .3746E-01  |
| .1147E+01 | .3507E+01 | -.1885E+01 | -.3867E+01 |
| .3857E+01 | .4900E+01 | .7187E+01  | .2308E+01  |
| .0000E+01 | .2007E+01 | .2684E-01  | .0000E+01  |
| .2917E+01 | .2840E+01 | -.2279E+01 | -.2710E+01 |
| .2604E+01 | .1807E+01 | -.7353E+01 | .3476E+01  |
| .3436E+01 | .9378E+00 | .1854E+01  | .1492E+01  |
| .0000E+01 | .4225E+01 | .1127E-01  | .0000E+01  |
| .4873E+01 | .2886E+01 | .5722E+01  | -.1135E+02 |
| .5604E+01 | .3343E+01 | -.4795E+01 | -.9104E+01 |
| .6000E+01 | .7255E+00 | -.3815E-01 | -.4172E-02 |
| .5697E+00 | .0000E+01 | .0000E+01  | .3508E-01  |
| .4199E+01 | .3707E+01 | .6784E+00  | .2036E+01  |
| .3871E+01 | .0000E+01 | .0000E+01  | .3834E-01  |
| .9915E+00 | .2427E+01 | -.1052E+02 | -.3906E+01 |
| .4185E+01 | .2749E+01 | .6578E+00  | -.3911E+01 |
| .3000E+01 | .4646E+01 | -.1763E+01 | -.1393E+02 |
| .4076E+01 | .9179E+00 | -.5160E+01 | .1919E+01  |
| .3252E+01 | .1860E+01 | -.2698E+01 | .2576E+01  |
| .3893E+01 | .3895E+01 | -.2993E+01 | .4964E+01  |
| .0000E+01 | .1747E+01 | .3380E-01  | .0000E+01  |
| .3509E+01 | .4625E+01 | .2334E+01  | .7943E+01  |
| .3562E+01 | .5499E+01 | -.9074E+01 | .7533E+01  |
| .2963E+01 | .6414E+00 | -.6271E+00 | -.1849E+01 |
| .1993E+01 | .2693E+01 | .7586E+00  | .4300E+01  |
| .1952E+01 | .6180E+00 | -.2222E+01 | -.3976E+01 |
| .7195E-05 | .3932E+01 | -.2531E+00 | .3071E-04  |
| .5347E+01 | .2084E+01 | -.5026E+01 | .5485E+01  |
| .6000E+01 | .4849E+00 | -.3815E-01 | .1490E-02  |
| .4065E+01 | .0000E+01 | -.4768E-02 | .1218E+00  |
| .1748E+01 | .3339E+00 | .1616E+01  | .1395E+01  |
| .4682E+01 | .1931E+01 | .1436E+01  | -.1915E+01 |
| .6000E+01 | .1217E+01 | -.2337E+00 | -.1192E-02 |
| .6569E+00 | .1557E+01 | -.7347E+01 | -.2864E+01 |
| .3745E+01 | .2753E+01 | -.9598E+01 | -.6806E+01 |
| .6074E+00 | .1236E+01 | -.9127E+01 | -.1446E+01 |
| .2901E+01 | .4179E+01 | .2306E-01  | .2060E+01  |
| .4237E+01 | .1193E+01 | .6797E+01  | -.3866E+01 |
| .2743E+01 | .9231E+00 | -.2862E+01 | .3147E+01  |
| .9555E+00 | .0000E+01 | -.5960E-03 | .3494E-01  |
| .1581E+01 | .1538E+01 | -.7691E+01 | .2351E+01  |
| .0000E+01 | .1235E+01 | .3991E-01  | -.3576E-02 |
| .5376E+01 | .1410E+01 | .2346E+01  | -.1820E+01 |
| .0000E+01 | .3365E+01 | .1647E-01  | -.2384E-02 |
| .1551E+01 | .3294E+01 | -.6013E+01 | .9090E+01  |
| .3081E+01 | .9408E+00 | .8184E+00  | -.1026E+01 |
| .1963E+01 | .1507E+01 | -.3086E+01 | -.3422E+01 |
| .8745E+00 | .6270E+00 | .2375E+01  | -.3142E+01 |
| .3091E+01 | .0000E+01 | -.2384E-02 | .3837E-01  |
| .5422E+01 | .0000E+01 | .0000E+01  | .1214E+00  |
| .3791E+01 | .1568E+01 | -.1177E+02 | -.7257E+00 |
| .2116E+01 | .0000E+01 | .0000E+01  | .3580E-01  |
| .4909E+01 | .5987E+00 | .4147E+00  | .1737E+01  |
| .5684E+00 | .6038E+00 | .4145E+00  | -.5575E+01 |
| .1728E+01 | .0000E+01 | .1192E-02  | .3845E-01  |

|           |           |            |            |
|-----------|-----------|------------|------------|
| .4391E+00 | .4889E+01 | -.8535E+01 | -.1211E+02 |
| .8691E+00 | .4938E+01 | -.6849E+01 | -.3219E+00 |
| .5455E+01 | .4597E+01 | .6163E+00  | -.1567E+02 |
| .1865E+01 | .2355E+01 | -.2551E+01 | -.1392E+01 |
| .2752E+01 | .3668E+01 | -.1034E+01 | -.5047E+01 |
| .0000E+01 | .7361E+00 | .4806E-01  | -.1192E-02 |
| .2345E+01 | .1525E+01 | .5190E+01  | .1658E+01  |
| .4359E+01 | .1972E+01 | -.2149E+01 | -.6530E+01 |
| .2318E+01 | .3618E+01 | -.9034E+00 | -.2596E+01 |
| .5300E+01 | .2436E+01 | .1848E+01  | .1693E+01  |
| .6000E+01 | .0000E+01 | -.1907E-01 | .7664E-02  |
| .2943E+01 | .1796E+01 | -.5467E+01 | .2587E+01  |
| .1973E+01 | .2060E+01 | .1663E+01  | -.1748E+01 |
| .3590E+01 | .1290E+01 | -.3345E+01 | -.3309E+01 |
| .4118E+00 | .4448E+01 | -.1320E+01 | -.6844E+01 |
| .3481E+01 | .8287E-05 | .1238E-03  | -.9105E+00 |
| .3181E+01 | .3913E+01 | -.8705E+00 | -.1697E+01 |
| .2033E+01 | .3344E+01 | -.1120E+02 | -.9535E+00 |
| .8029E+00 | .3908E+01 | -.3372E+01 | .1129E+01  |
| .5579E+01 | .2979E+01 | .6705E+01  | .2812E+01  |
| .1206E+01 | .3945E+01 | .1716E+01  | .6876E+00  |
| .4453E+01 | .0000E+01 | -.4768E-02 | .4062E-01  |
| .2113E+01 | .3495E+00 | -.6682E+00 | -.3848E+01 |
| .1864E+01 | .4420E+01 | .8952E+01  | .9155E+00  |
| .2287E+01 | .6198E+00 | -.3119E+01 | -.8433E+01 |
| .1351E+01 | .1818E+01 | -.6449E+01 | -.8989E+00 |
| .1828E+01 | .3692E+01 | -.2743E+01 | -.6424E+01 |
| .3537E+00 | .2811E+01 | -.3089E+00 | .9033E+01  |
| .4458E+00 | .3949E+01 | -.5335E+01 | -.5013E+00 |
| .7566E+00 | .3166E+01 | .1846E+01  | -.9687E+00 |
| .7910E+00 | .5500E+01 | -.4167E+01 | -.4329E-02 |
| .5228E+01 | .0000E+01 | -.4768E-02 | .4032E-01  |
| .3903E+01 | .1234E+01 | .1533E+00  | -.5116E+01 |
| .3590E+01 | .3710E+01 | .1837E+01  | -.4083E+00 |
| .3320E+00 | .2412E+01 | -.6858E+01 | -.4595E+01 |
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| .4416E+01 | .1654E+01 | -.2214E+01 | -.3468E+01 |
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| .5160E+01 | .5497E+01 | -.1058E+02 | .1012E+02  |
| .0000E+01 | .4906E+00 | .3586E-01  | -.2980E-02 |
| .3150E+01 | .3544E+01 | -.2923E+01 | -.7726E+01 |
| .2091E+01 | .9200E+00 | -.6836E+00 | -.3234E+00 |
| .0000E+01 | .3087E+01 | .2055E-01  | -.2384E-02 |
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| .3783E+00 | .0000E+01 | -.8941E-03 | .3522E-01  |
| .5102E+01 | .4011E+01 | .2967E+01  | -.6725E+01 |
| .1823E+01 | .1231E+01 | -.7980E+01 | -.7574E+01 |
| .2875E+01 | .1219E+01 | -.1684E+01 | -.1697E+01 |
| .1014E+01 | .1710E+01 | -.5619E+01 | .1552E+01  |
| .4712E+01 | .1560E+01 | .6130E+00  | -.1587E+01 |
| .2996E+00 | .1390E+01 | -.7407E+01 | .2492E+01  |

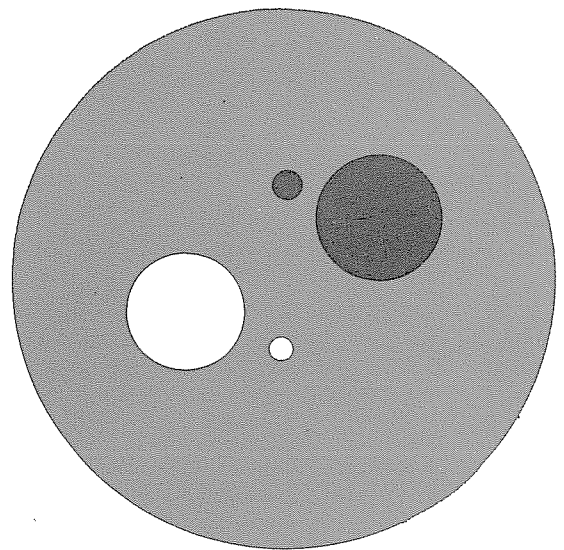
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| .4424E+01 | .4364E+01 | .1122E+00  | -.1598E+02 |
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| .3250E+00 | .1079E+01 | -.4566E+01 | -.8678E+00 |
| .3317E+01 | .2160E+01 | -.1664E+01 | -.9306E+01 |
| .3891E+01 | .4375E+01 | -.1157E+02 | .5004E+01  |
| .2399E+01 | .2656E+01 | .6614E+01  | -.7863E+00 |
| .2234E+01 | .4854E+01 | .7512E+01  | .8386E+01  |
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| .5043E+01 | .9060E+00 | -.5321E+01 | -.3760E+01 |
| .9346E+00 | .1396E+01 | -.5883E+01 | -.2084E+01 |
| .3594E+01 | .6173E+00 | -.2531E+01 | -.8318E+01 |
| .0000E+01 | .4532E+01 | .1333E-01  | .4768E-02  |
| .2747E+01 | .2561E+01 | .3881E+01  | -.8888E+01 |
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| .6577E+00 | .2644E+01 | -.8430E+00 | .4107E+01  |
| .6000E+01 | .2438E+00 | -.5722E-01 | .1043E-02  |
| .4841E+01 | .0000E+01 | -.4768E-02 | .4140E-01  |
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| .2782E+01 | .3617E+00 | -.1751E+01 | -.2918E+01 |
| .9063E+00 | .2820E+01 | -.6684E+01 | -.1284E+01 |
| .4870E+01 | .3254E+01 | -.2680E+01 | -.4642E+01 |
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| .2487E+01 | .3309E+01 | .1769E+01  | .1396E+01  |
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| .5245E+01 | .3162E+01 | -.5381E+01 | -.1751E+01 |
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| .4259E+01 | .0000E+01 | -.4768E-02 | .3677E-01  |
| .3988E+01 | .3001E+01 | .2189E+01  | -.8043E+01 |
| .5348E+01 | .1728E+01 | -.8095E+01 | -.6193E+01 |
| .3951E+01 | .3402E+01 | -.7387E+01 | -.2373E-01 |
| .1472E+01 | .4610E+01 | .1191E+02  | -.1304E+01 |

|           |           |            |            |
|-----------|-----------|------------|------------|
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| .6000E+01 | .2237E+01 | -.3338E-01 | -.2384E-02 |
| .5390E+01 | .9465E+00 | -.5408E+00 | -.7687E+00 |
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| .3195E+01 | .3124E+01 | -.3099E+01 | -.1217E+02 |
| .1170E+01 | .4344E+01 | -.4107E+00 | -.7111E+01 |
| .1784E+01 | .5296E+01 | .8742E+01  | -.8255E+01 |
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| .0000E+01 | .5294E+01 | .1376E-01  | .0000E+01  |
| .5514E+01 | .5273E+01 | -.7565E+00 | .1294E+01  |
| .3419E+00 | .5472E+01 | .1116E+02  | -.1295E+01 |
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| .5572E+01 | .4176E+01 | .6726E-01  | .5108E+00  |
| .4626E+01 | .5322E+01 | .8750E+01  | -.9769E+00 |
| .6000E+01 | .5500E+01 | -.9537E-02 | -.9537E-02 |

# COMPUTER SCIENCES DEPARTMENT

University of Wisconsin-  
Madison



## NEW INVESTIGATIONS OF VON NEUMANN TYPE FLUIDS

by

Craig L. Hougum

and

Donald Greenspan

Computer Sciences Technical Report #323

May 1978